

High power, high intensity superconducting proton driver linac at KEK

High Energy Accelerator Research Organization

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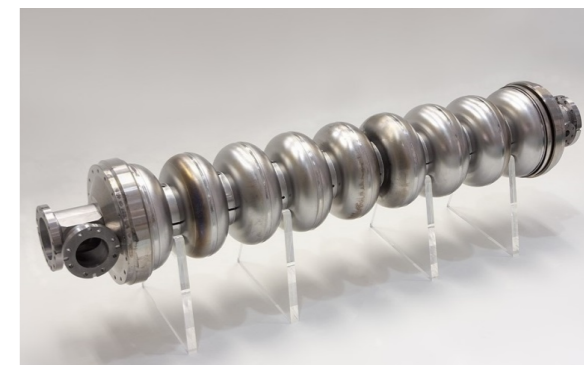
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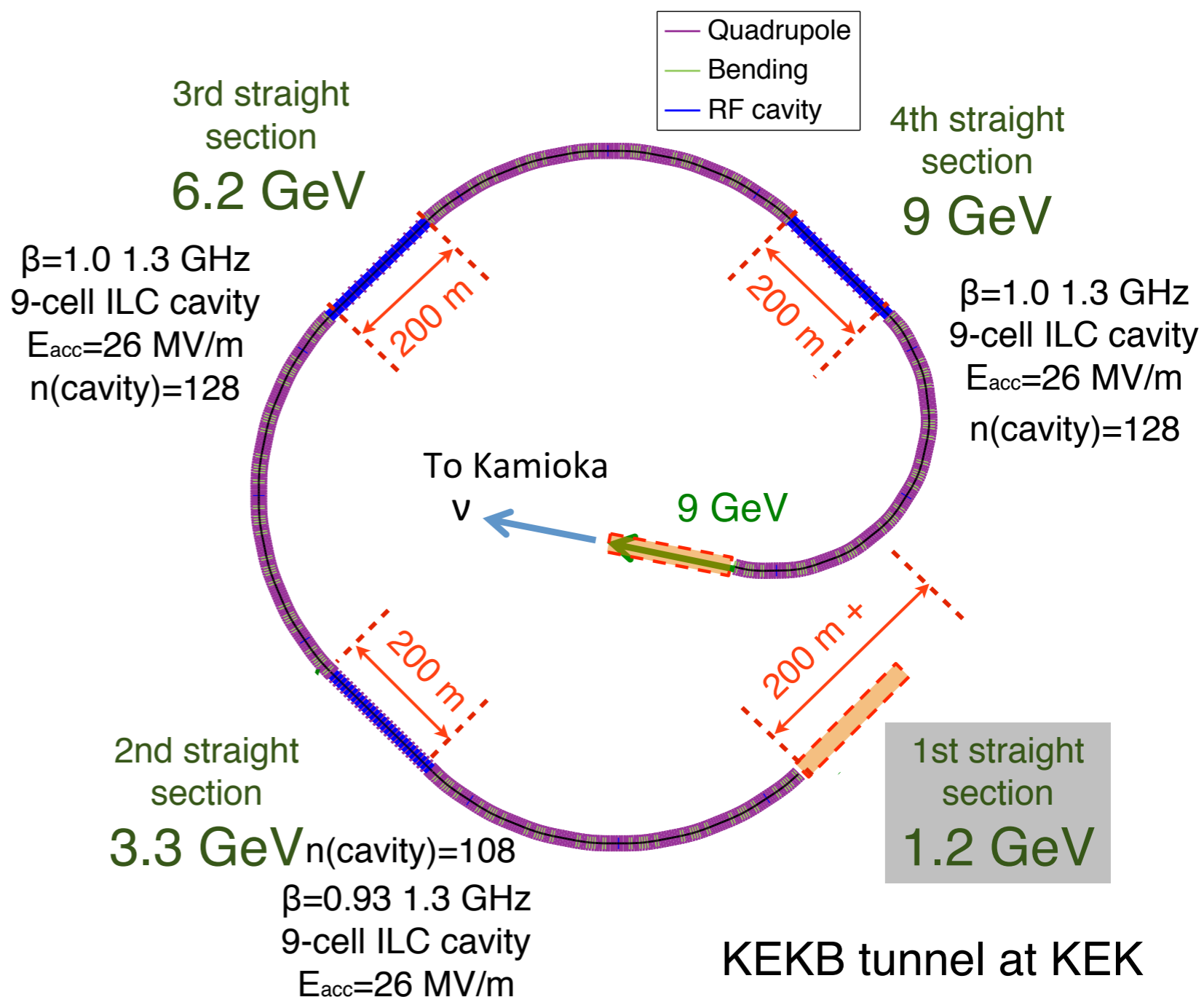
Proton driver linac overview

- For long-baseline neutrino oscillation physics, multi-MW proton driver linac with high intensity beam current is needed.
- For efficient acceleration, linac is operated in pulsed mode with high duty

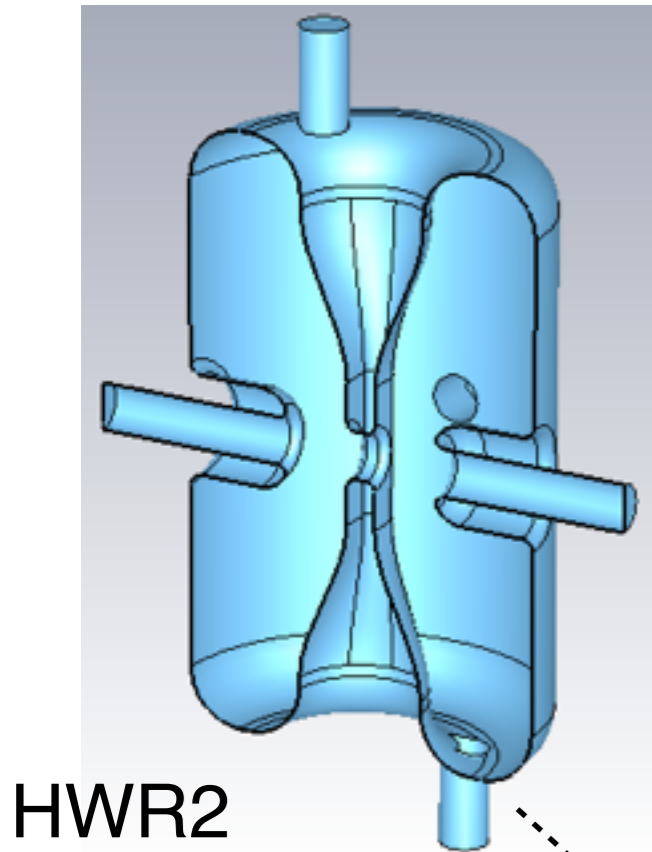
ILC 9-cell elliptical cavity



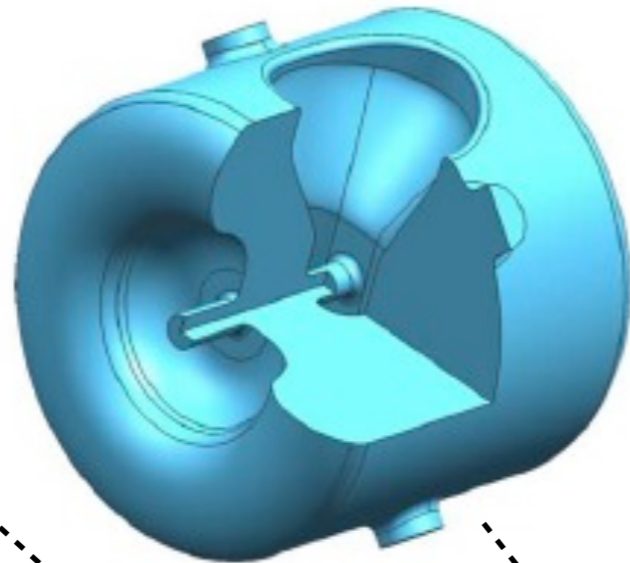
Beam parameters	Value
Beam energy	9 GeV
(peak) Beam current	100 mA
Repetition rate	10 Hz
Pulse length	1 ms
Average beam current	1mA
Beam power	9 MW



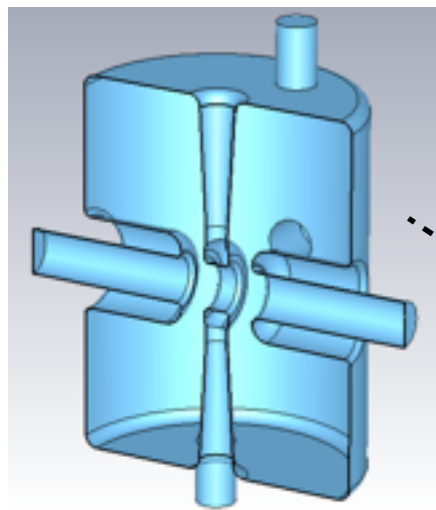
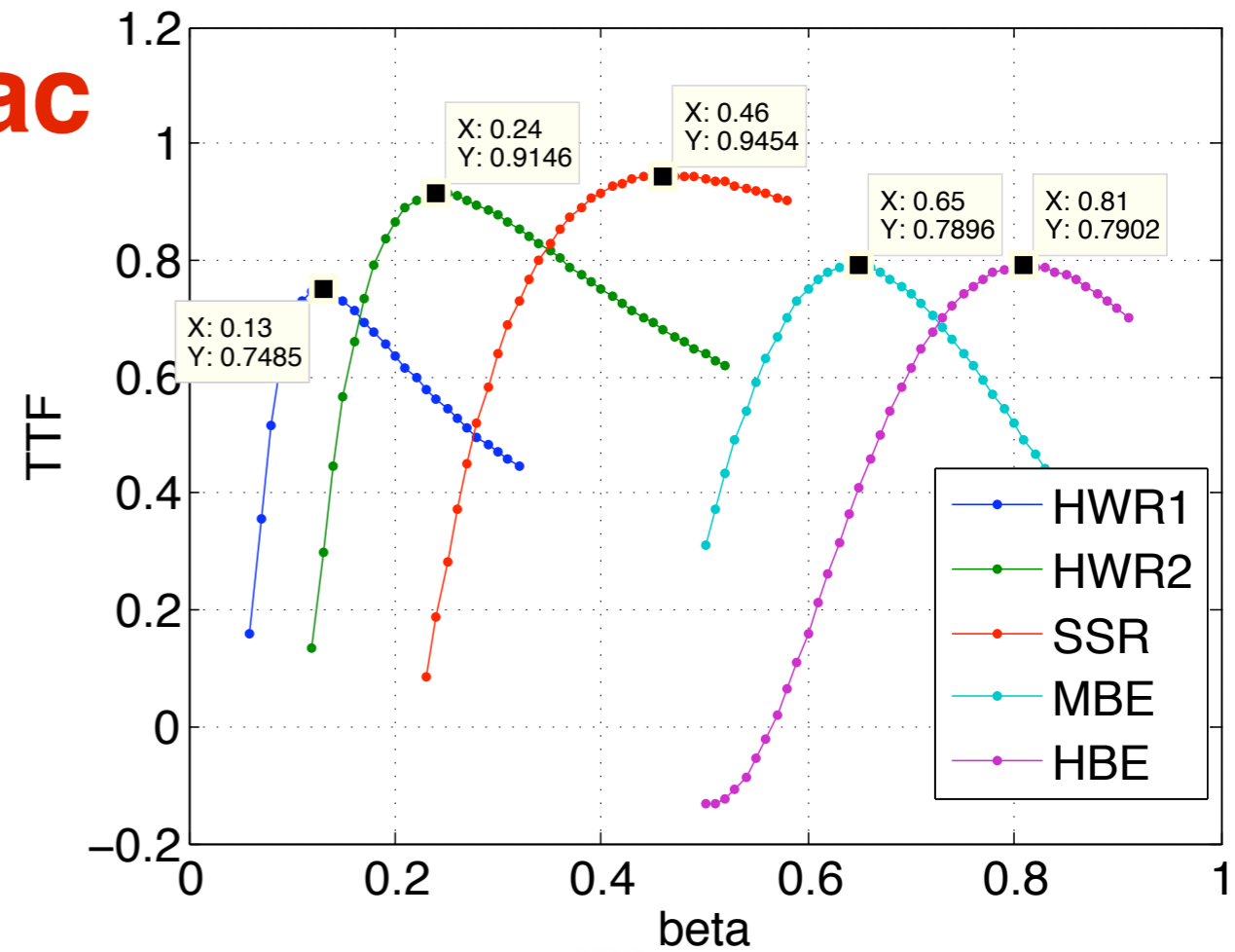
Front-end linac



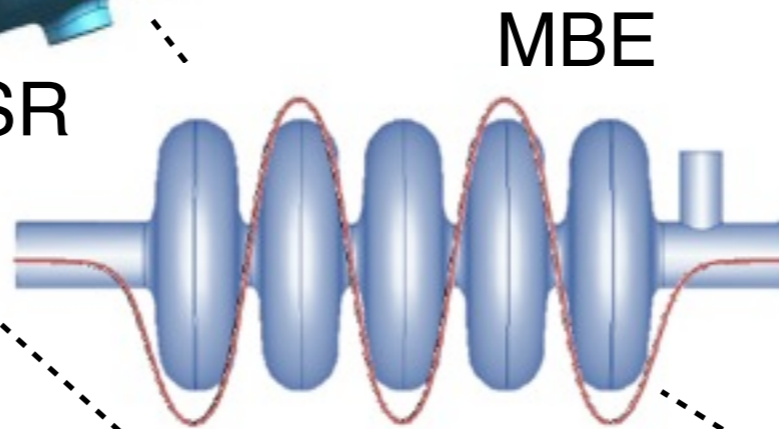
HWR2



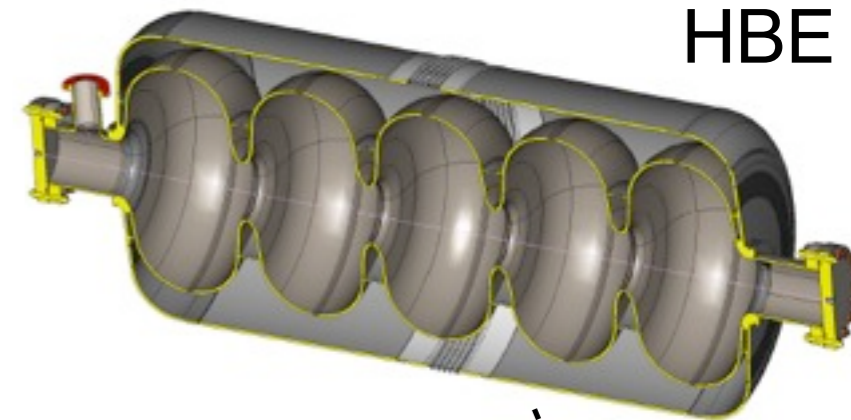
SSR



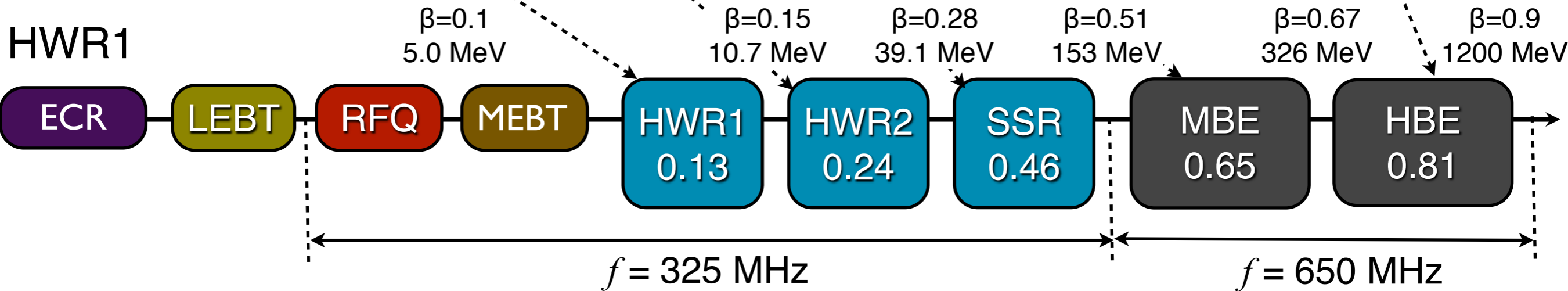
HWR1



MBE



HBE



Linac structure: cryomodule



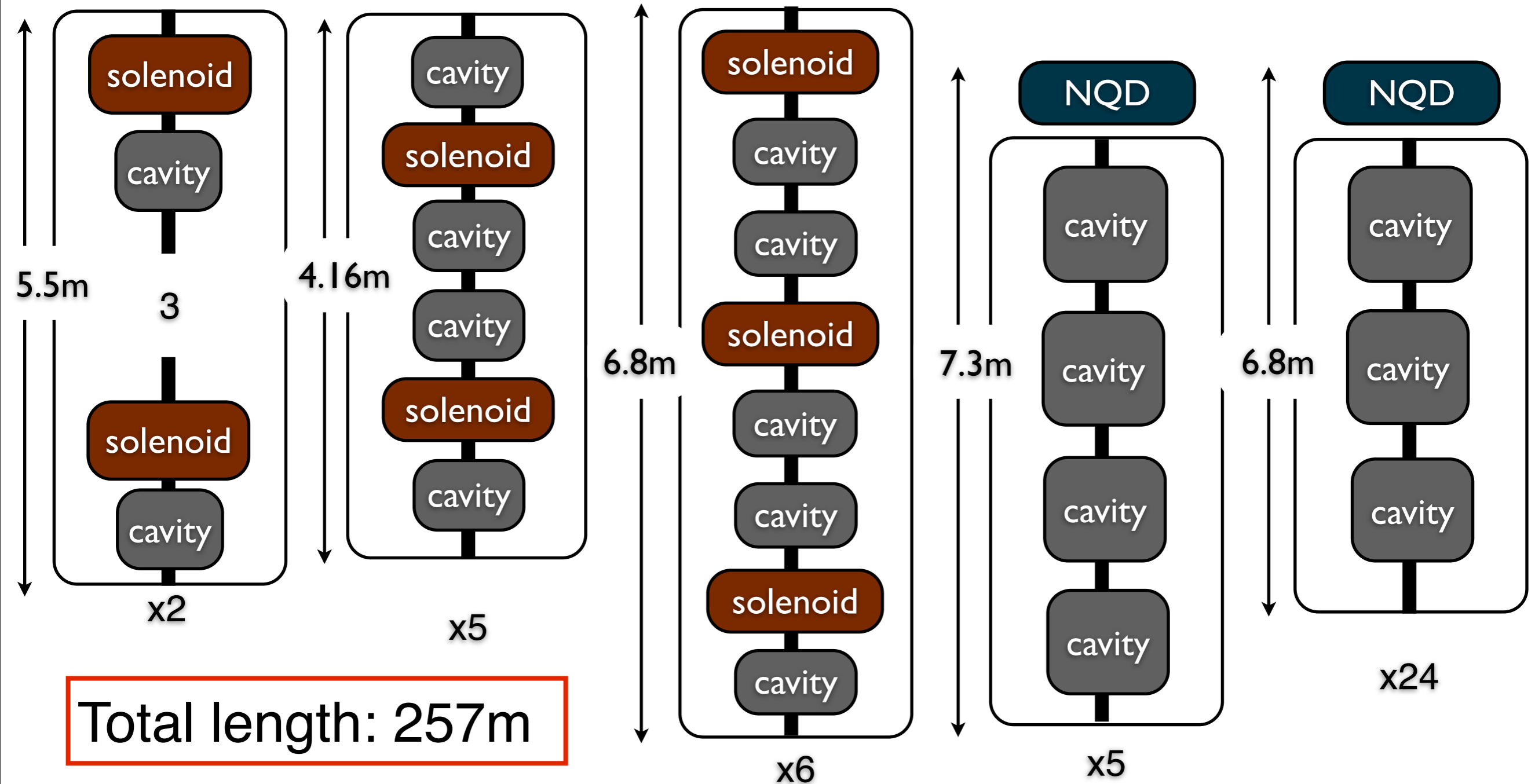
c: 330 mm
ss: 400 mm
t: 170 mm

c: 500 mm
ss: 480 mm
t: 200 mm

c: 750 mm
ss: 480 mm
t: 200 mm

c: 727 mm
t: 500 mm
e: 2890 mm

c: 946 mm
t: 504mm
e: 2890 mm



Front end component specification

cavities	HWR1	HWR2	SSR	MBE	HBE
n (cell/gap)	2	2	2	5	5
f (MHz)	325	325	325	650	650
β_{opt}	0.13	0.24	0.46	0.65	0.81
E_{in} (MeV)	0.10	0.15	0.29	0.51	0.67
E_{out} (MeV)	0.15	0.29	0.51	0.67	0.9
V_0 (MV)	0.8	2.1	5.3	10.2	15.4
synchronous phase ($^{\circ}$)	-30	-30	-27	-25	-25
P_{beam} (peak) (MW)	0.052	0.167	0.447	1.02	1.54
n (cavity)	10	20	30	20	72
n (cryomodule)	2	5	6	5	24

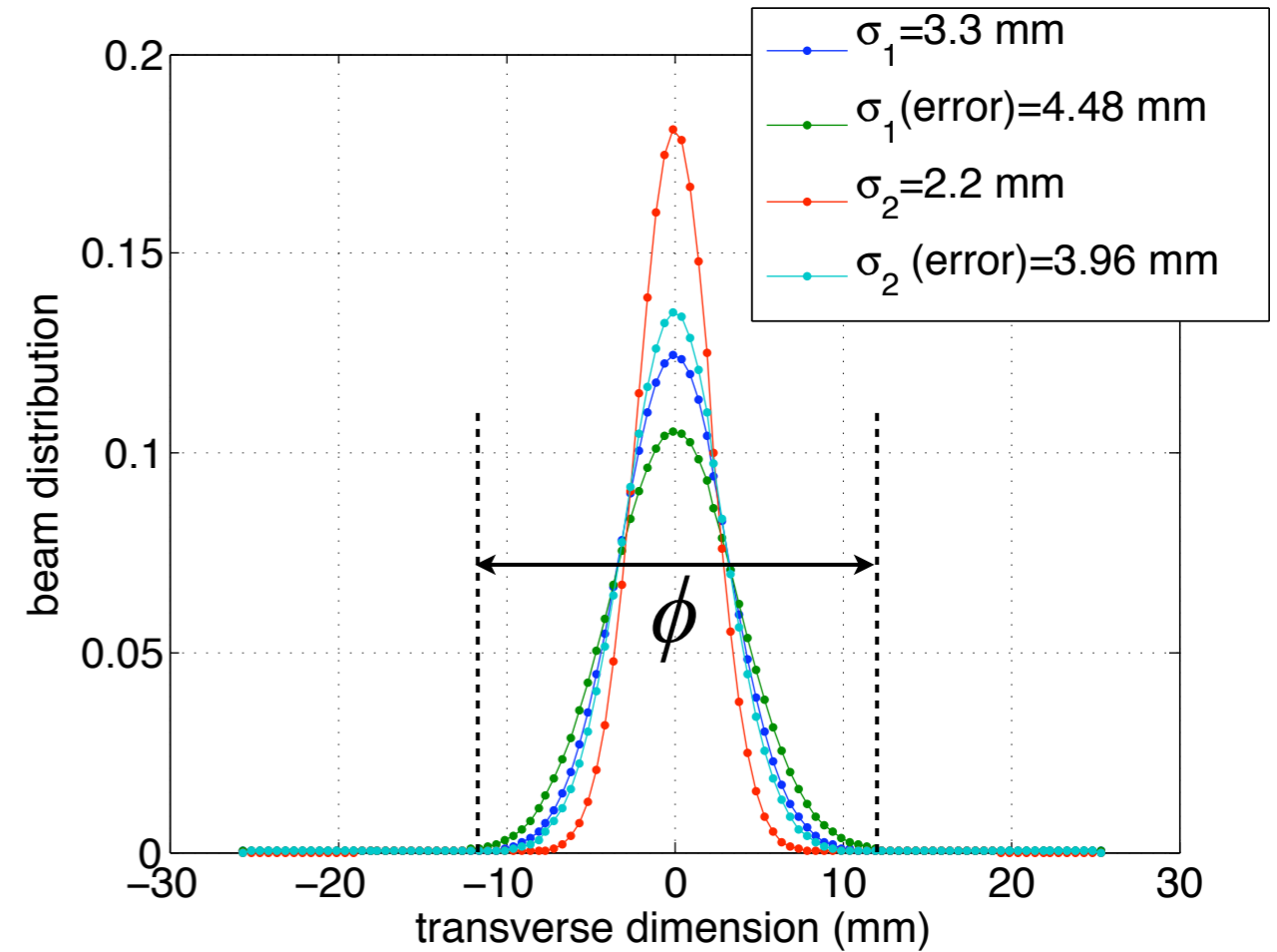
Development of two superconducting half wave resonators

- Requirements from beam dynamics

Specification	HWR1	HWR2
f (MHz)	325	325
β_{opt}	0.13	0.24
ϕ (mm)	40	40

- Other considerations

must come with superconducting solenoid for tight focusing. \rightarrow axis-symmetric accelerating gradient



Specification	HWR1	HWR2
σ (mm)	3.2	2.2
P_b (W)	5.50E+04	1.40E+05
loss rate	1.80E-05	7.10E-06
aperture	$\pm 4.4\sigma$	$\pm 4.9\sigma$
error margin	1.4	1.8
ϕ (mm)	40	40

Important features of the cavities

HWR1

HWR2

Frequency control

100 mm

Tapering

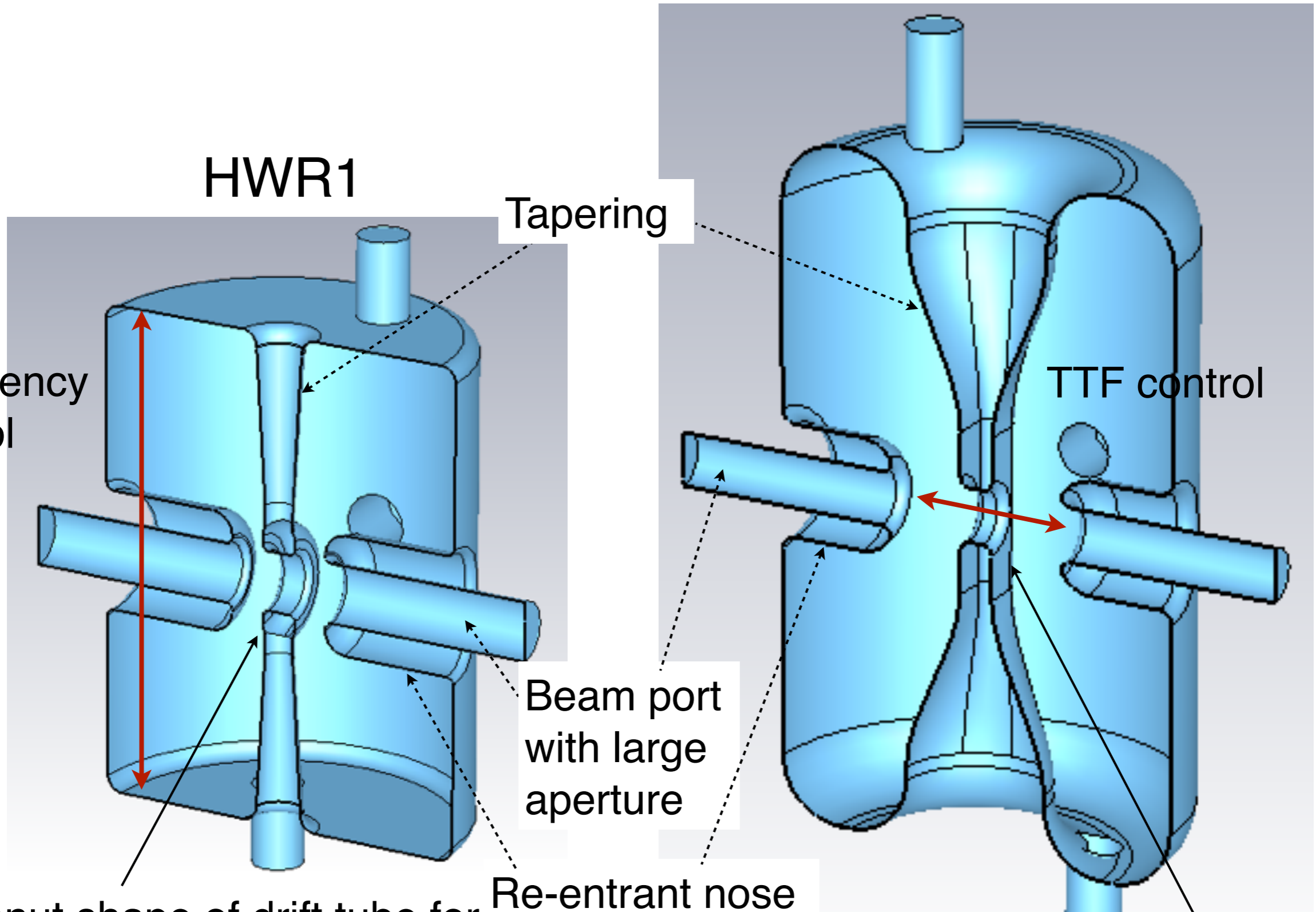
TTF control

Beam port with large aperture

Re-entrant nose

The donut shape of drift tube for axis-symmetric accelerating field

The race-track shape for higher accelerating gradient.

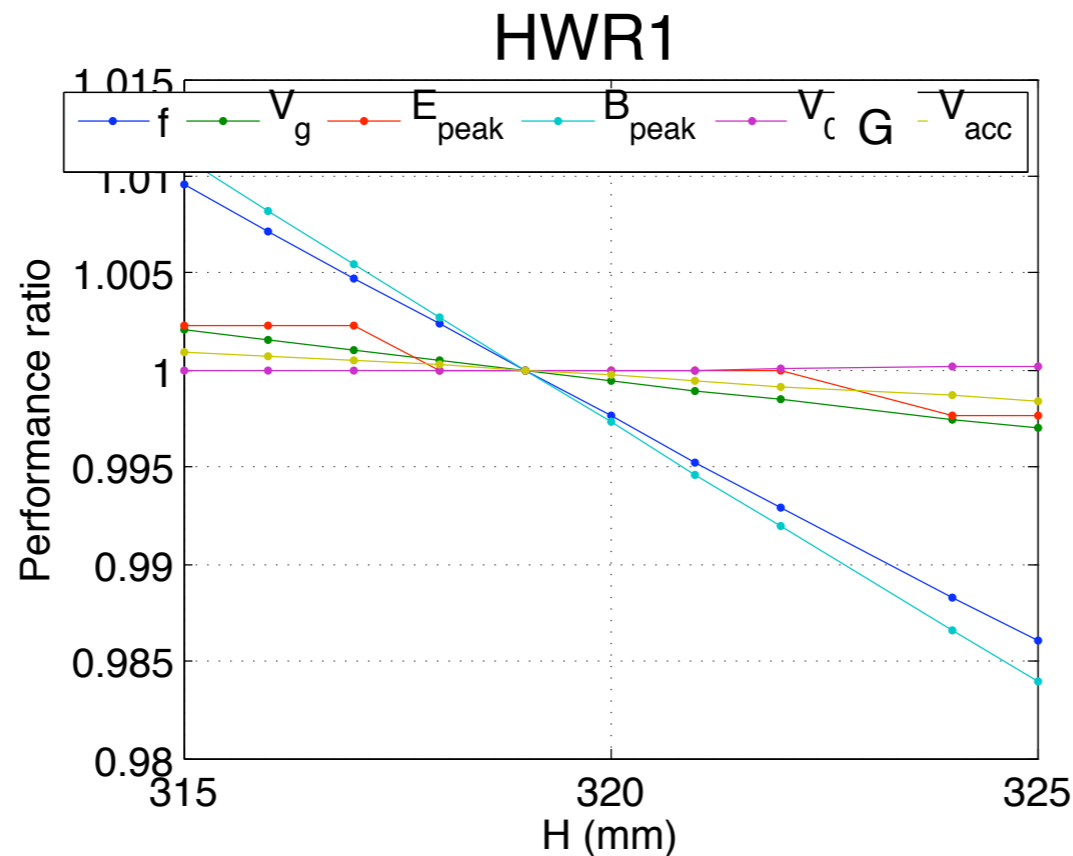
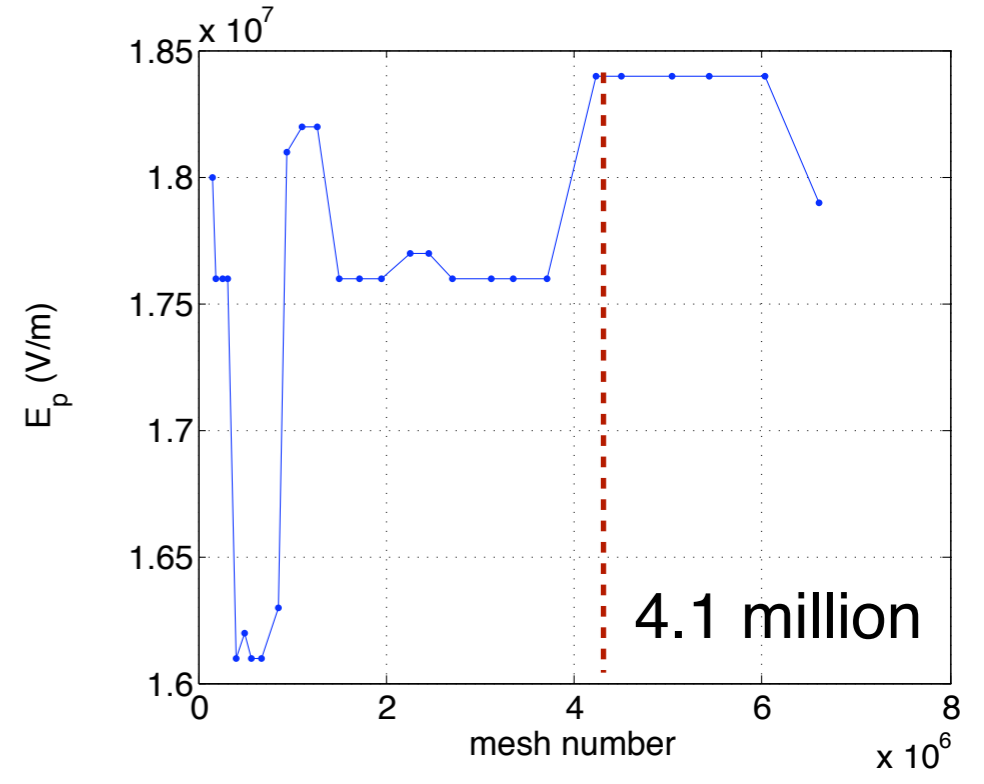
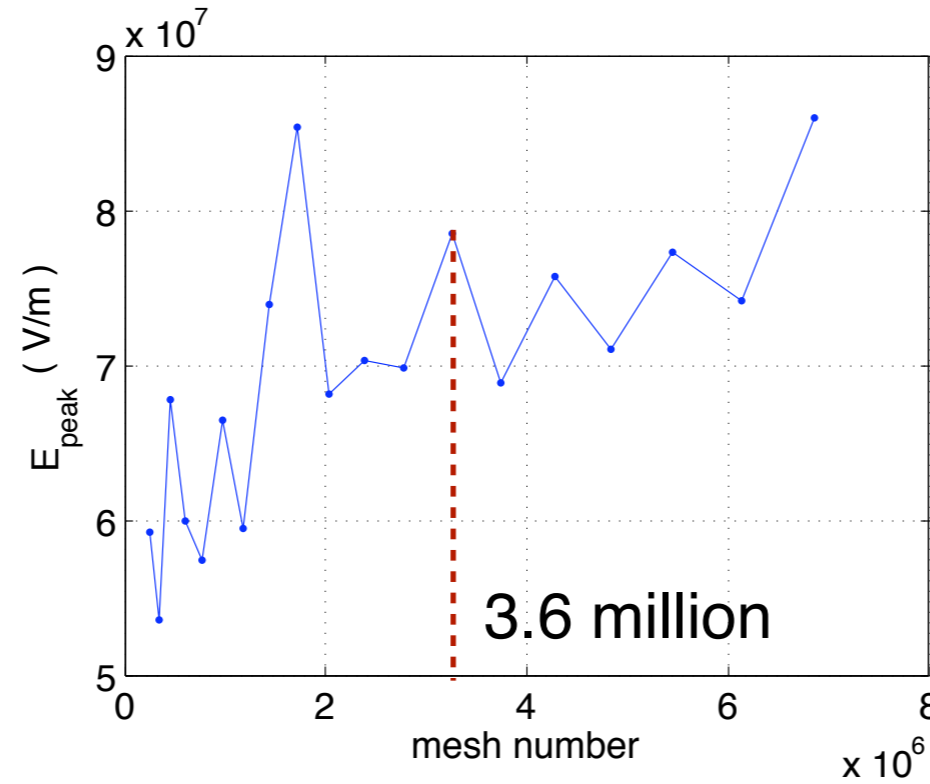


Optimization of cavity geometry

Figures of merit

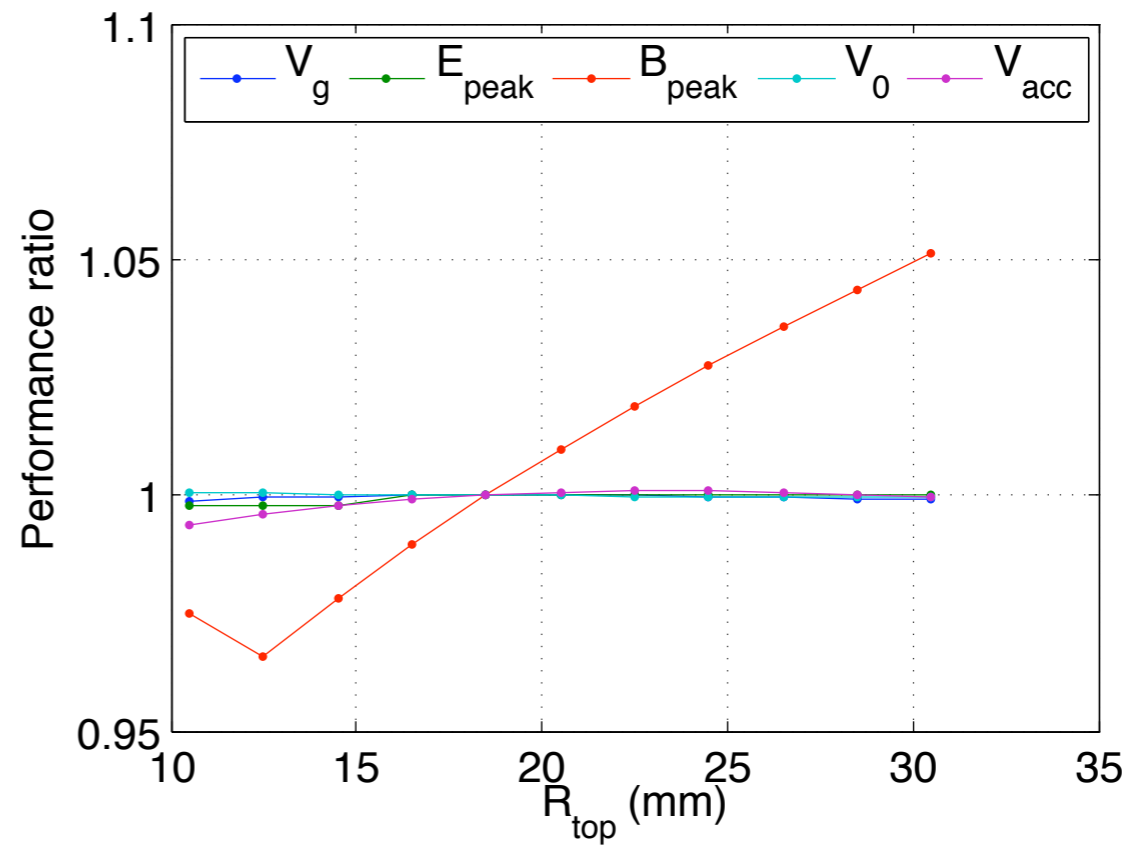
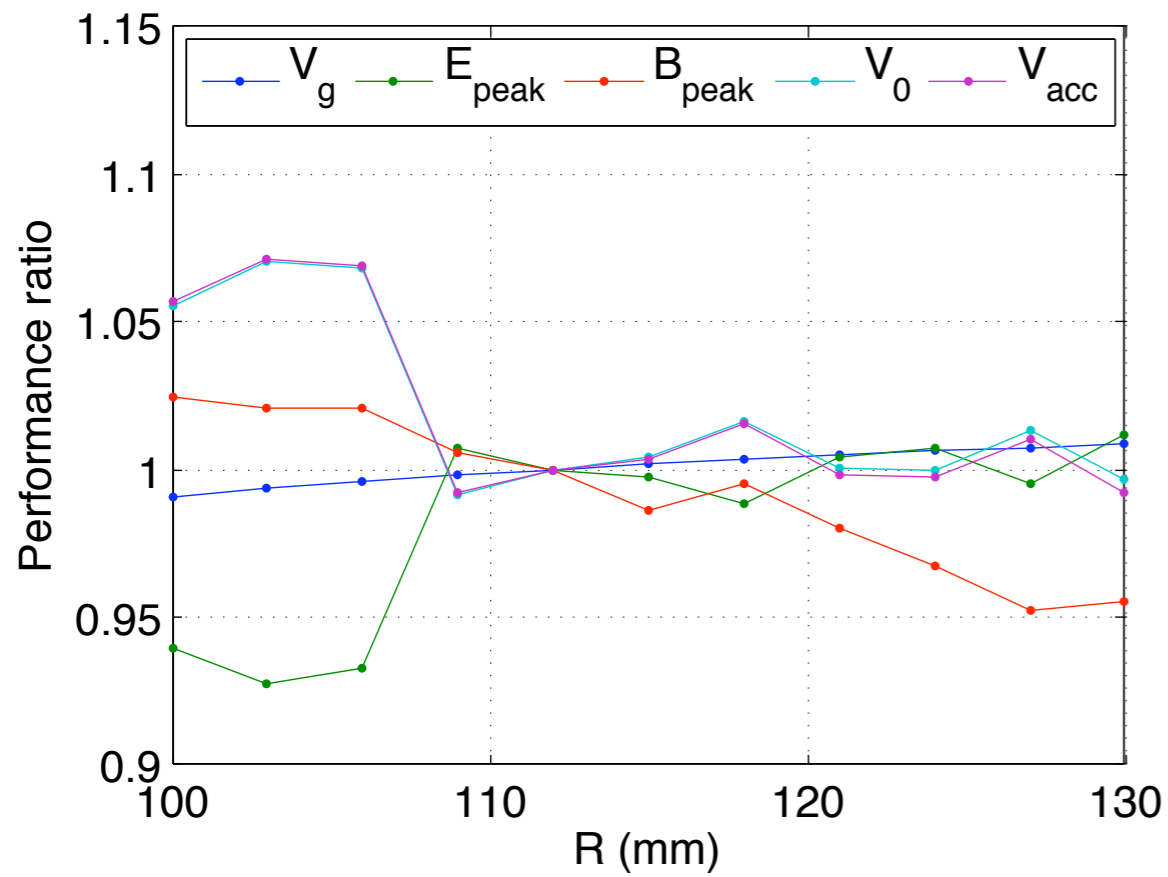
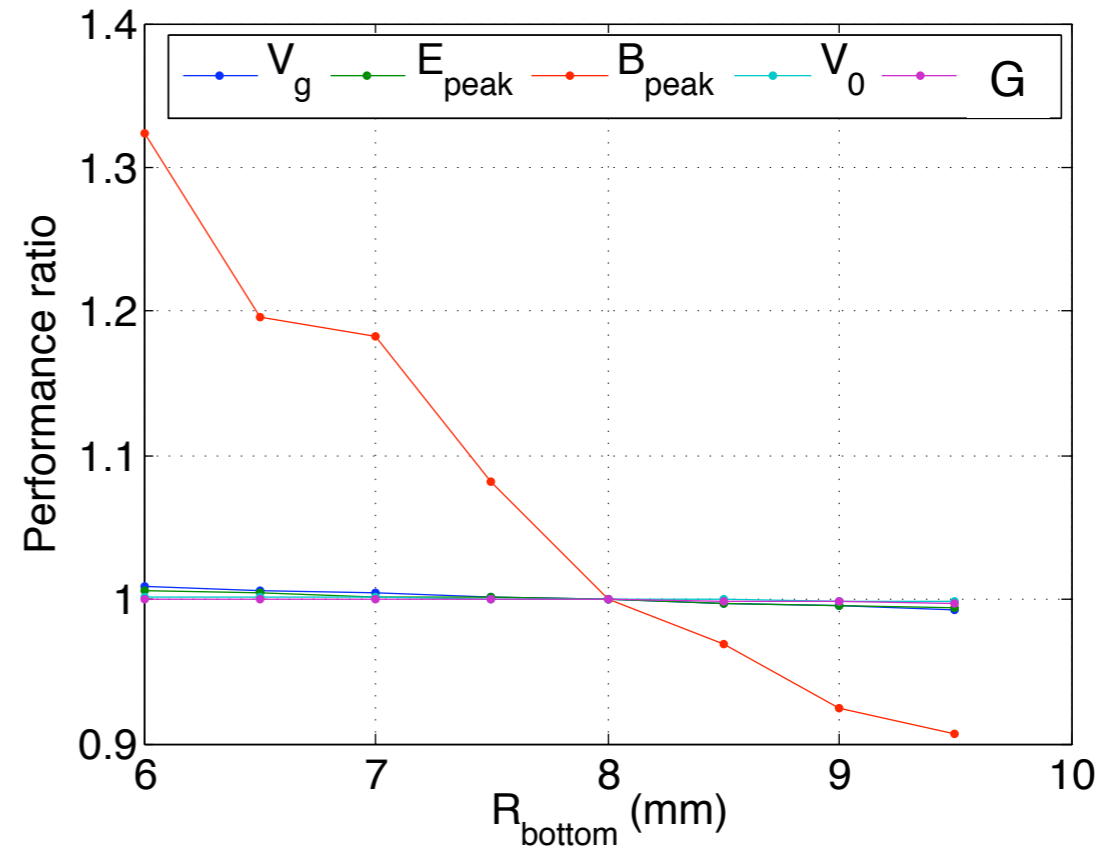
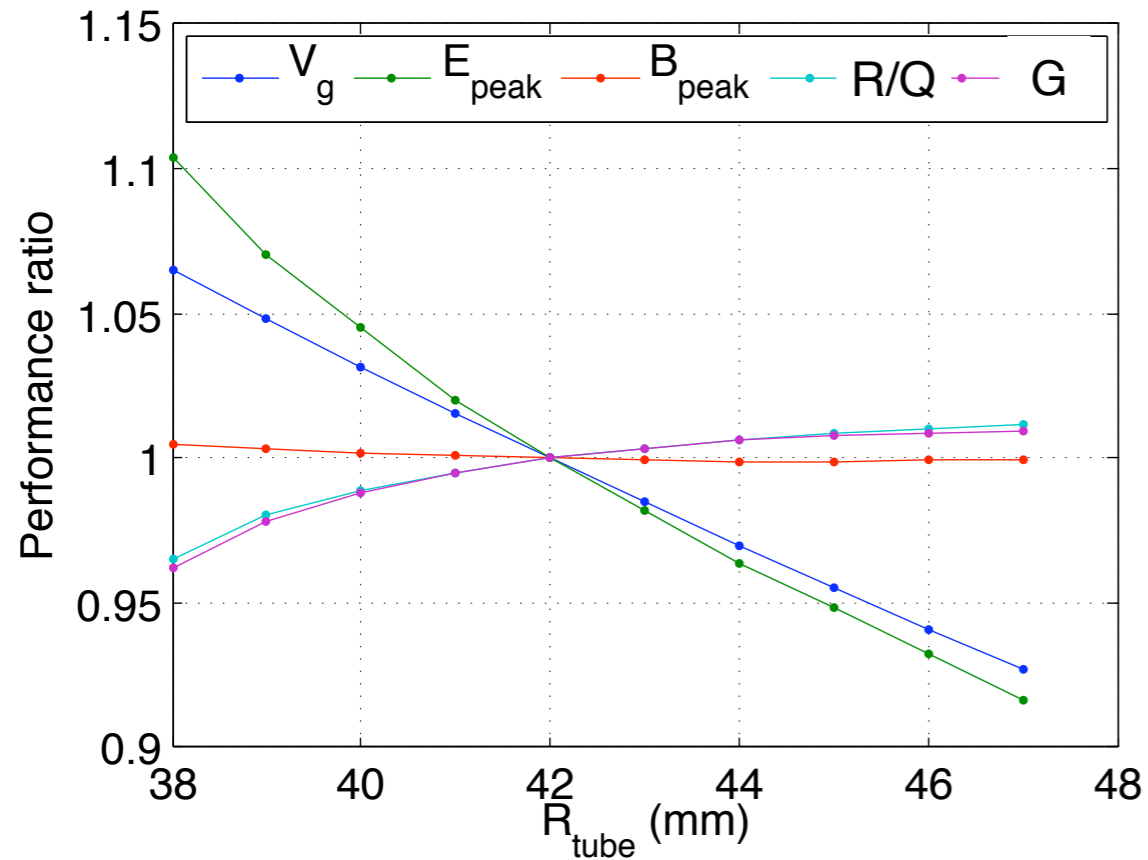
f (resonant frequency)
TTF (transit time factor)
R/Q [β] (shunt impedance)
G (geometrical factor)
B_{sp} / E_{acc}
E_{sp} / E_{acc}

• E_p vs mesh number

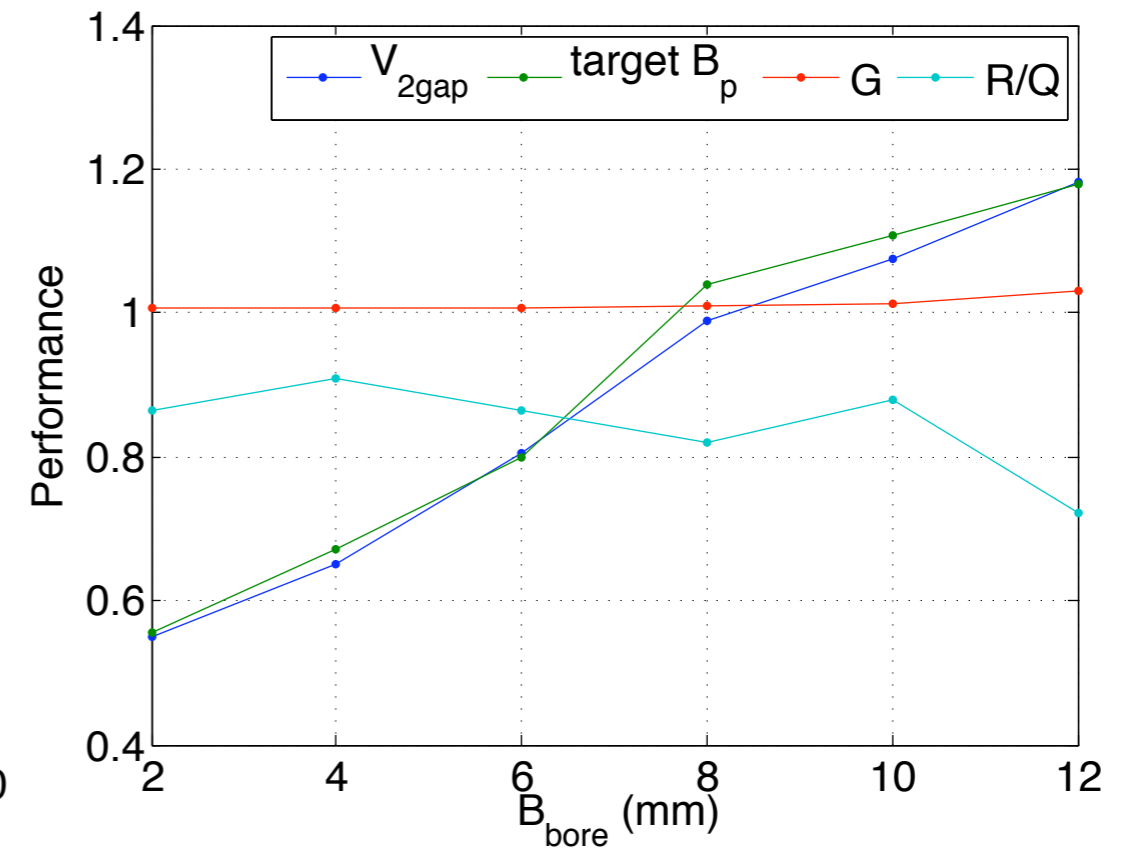
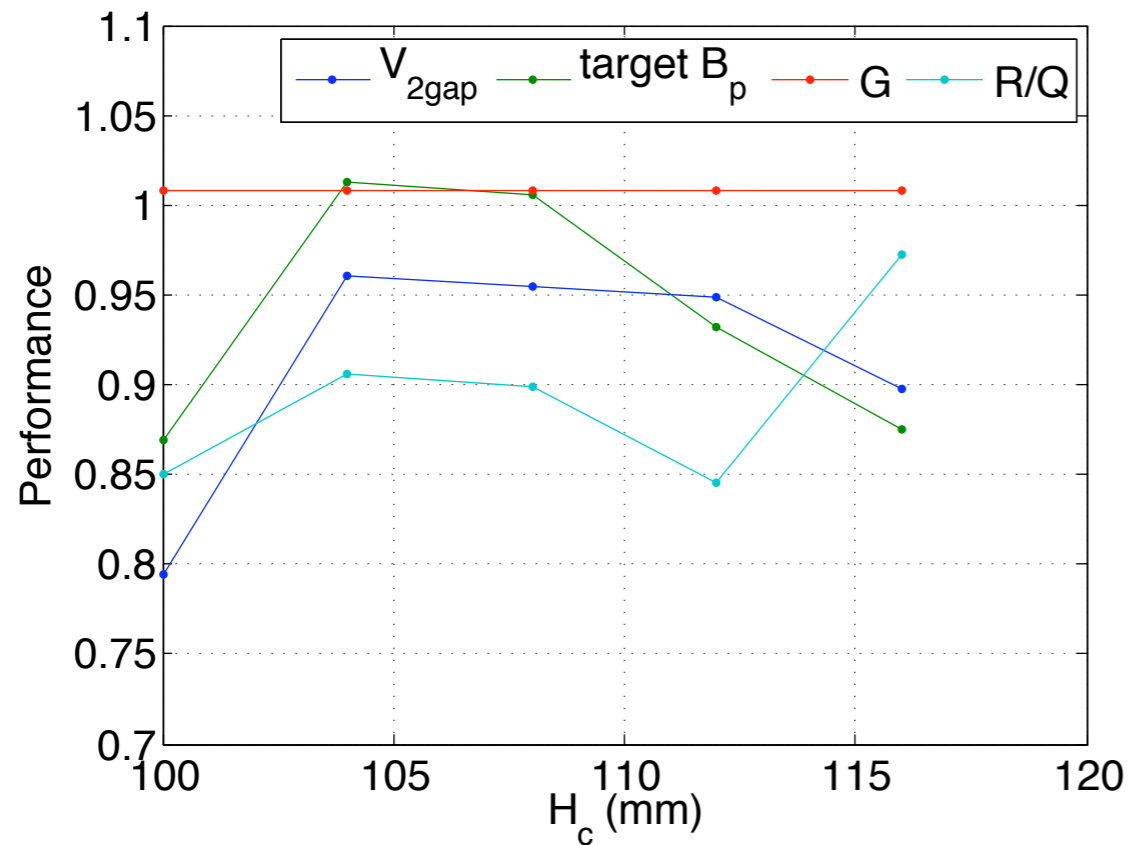
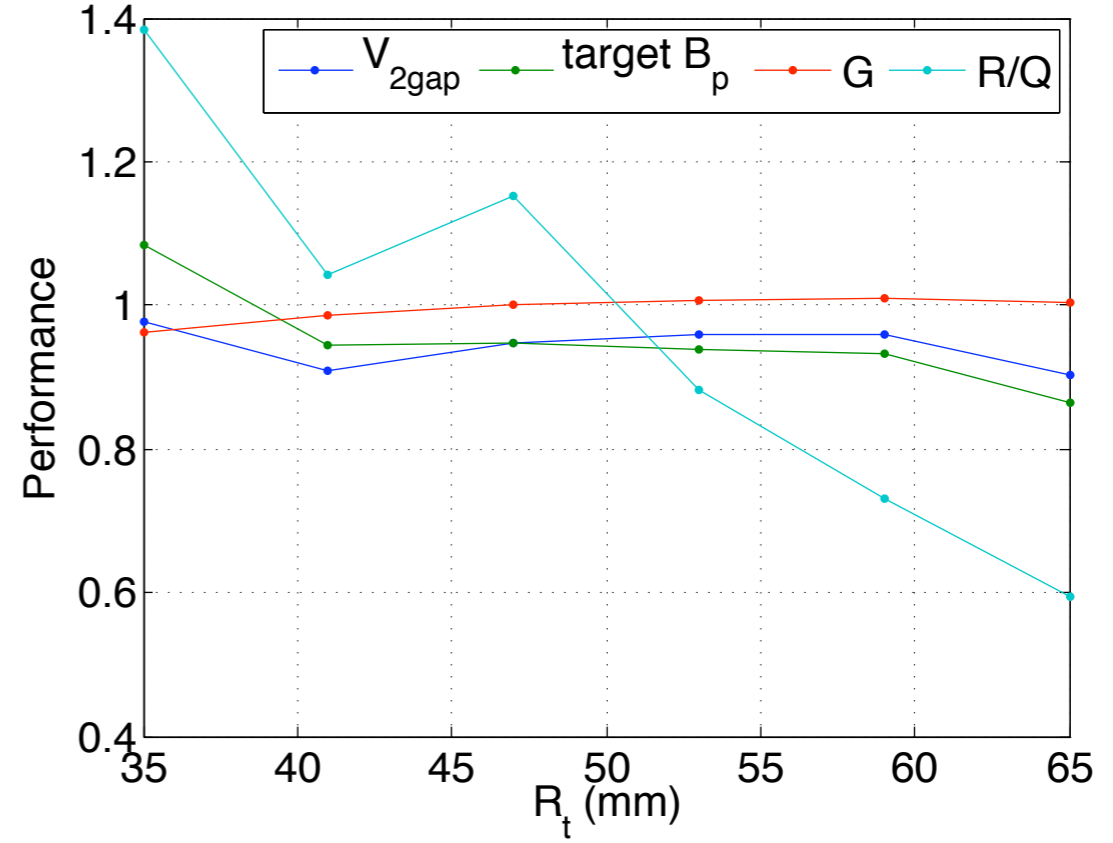
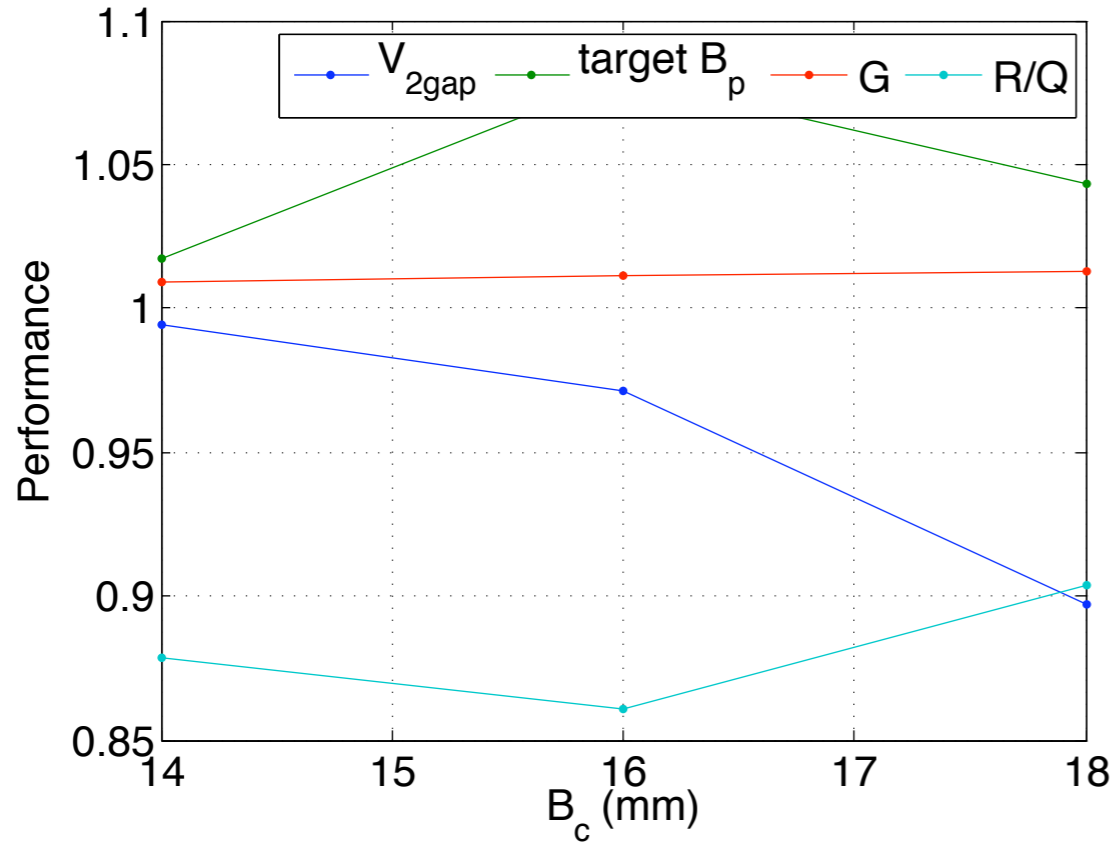


frequency was controlled by height

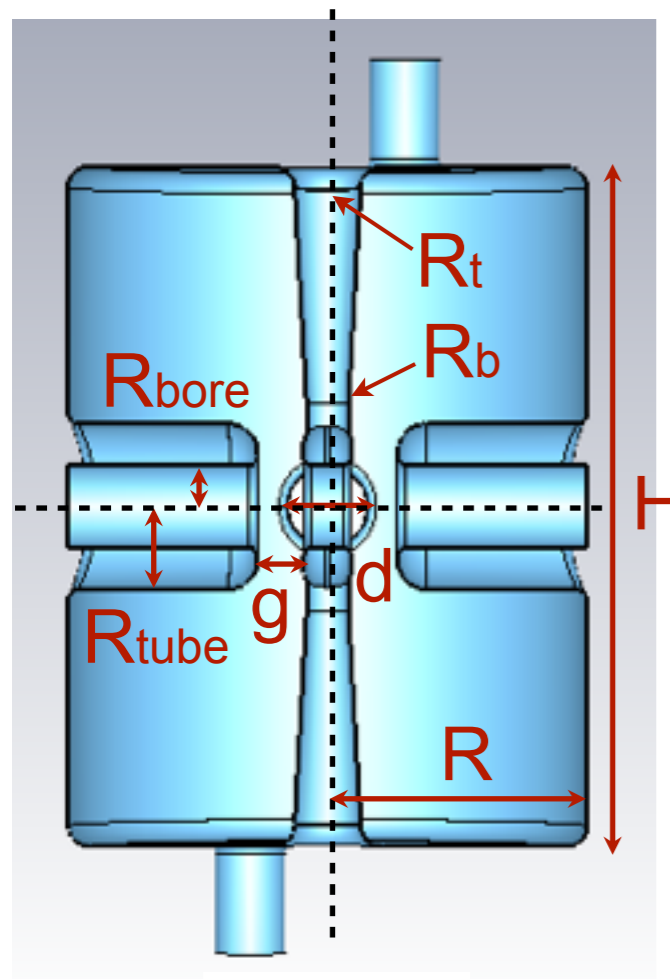
HWR1



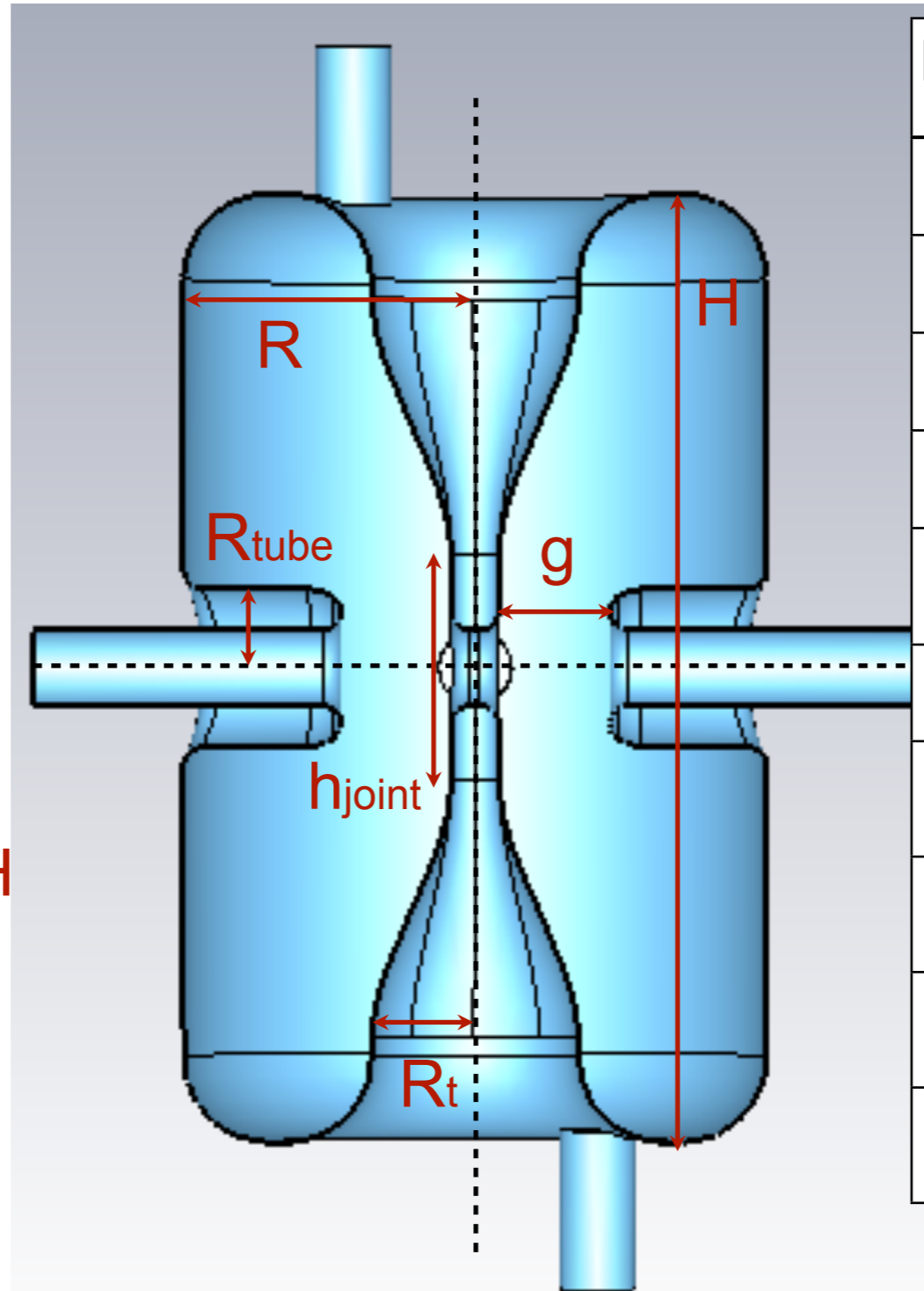
HWR2



Dimensions of the cavities



HWR1



HWR2

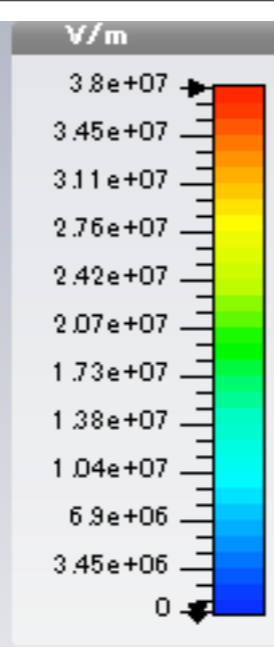
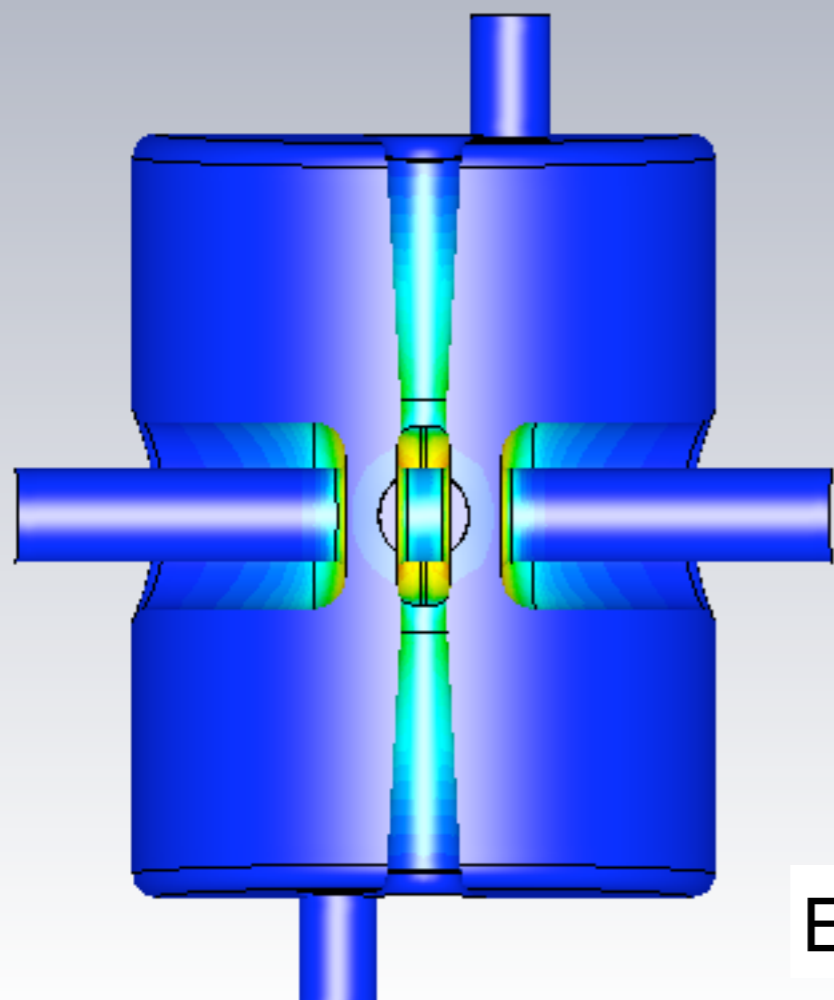
Parameters	HWR1	HWR2
H (mm)	332	503
d (mm)	45	77
g (mm)	22	52
R (mm)	125	155
R _{tube} (mm)	40	42
R _t (mm)	16	55
R _b (mm)	10	80
R _{bore} (mm)	20	20
h _{tune} (mm)	1	10
h _{joint} (mm)	10	120

RF performance of the cavities

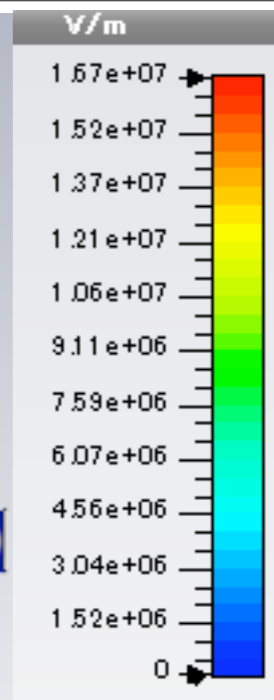
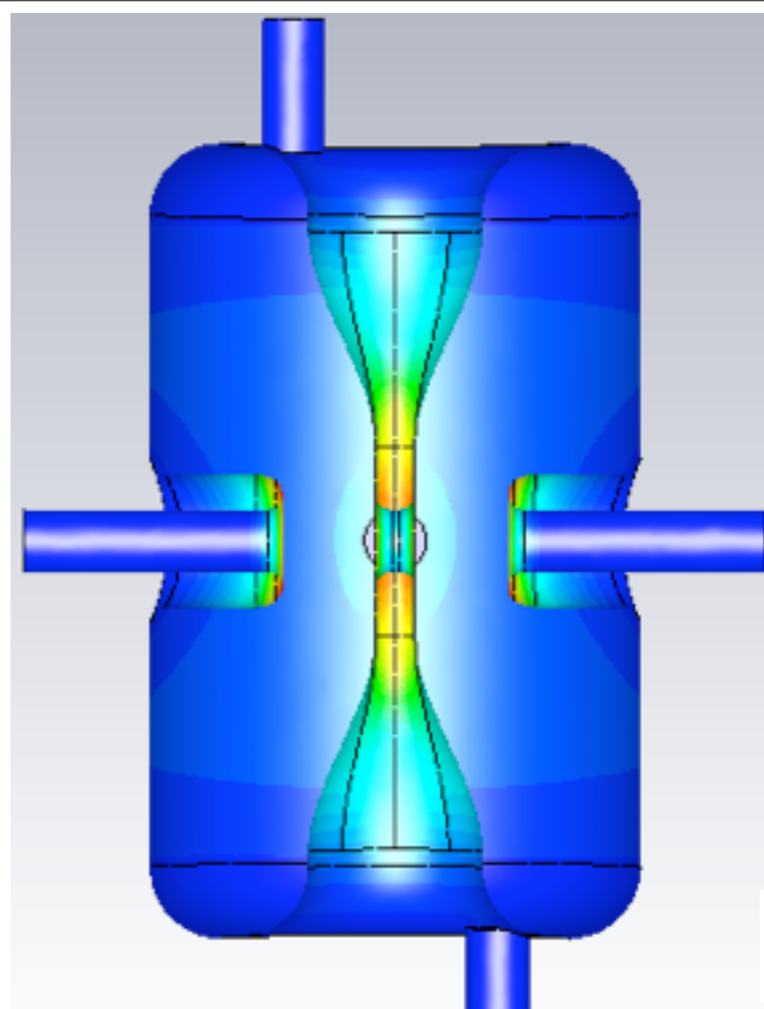
surface resistance for high purity Nb

$$R_s (4K) = 47.4 \text{ n}\Omega$$

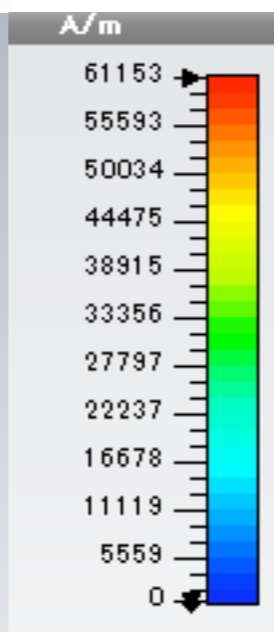
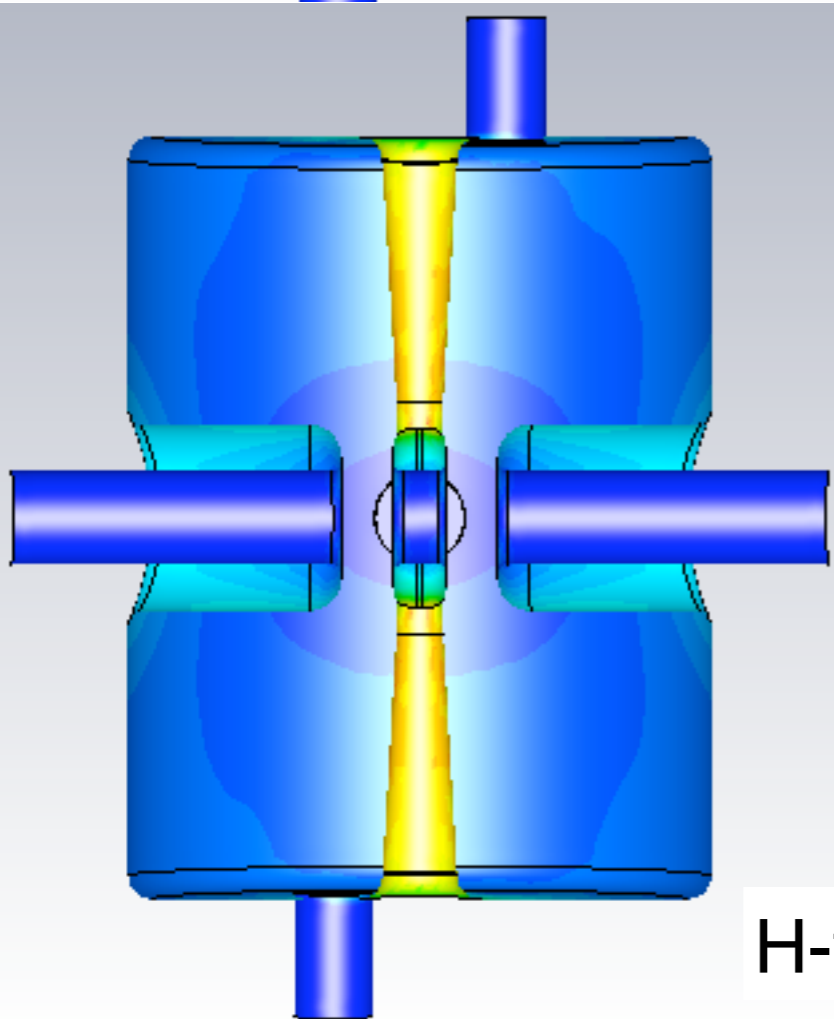
Figures of merit	HWR1	HWR2
V_0	0.86 MV	1.93 MV
TTF	0.77	0.79
V_{acc}	0.66 MV	1.52 MV
E_{acc}	5.5 MV/m	6.9 MV/m
R/Q_0	237.7 Ω	120.8 Ω
G	53.8 Ω	88.3 Ω
Q_0	1.10E+09	1.90E+09
U	0.9 J	4.4 J
P_{wall}	1.6 W	4.8 W
E_{sp}/E_{acc}	6.3	5.1
B_{sp}/E_{acc}	12.9 (mT/(MV/m))	8.3 (mT/(MV/m))
P_g	57 kW	132 kW



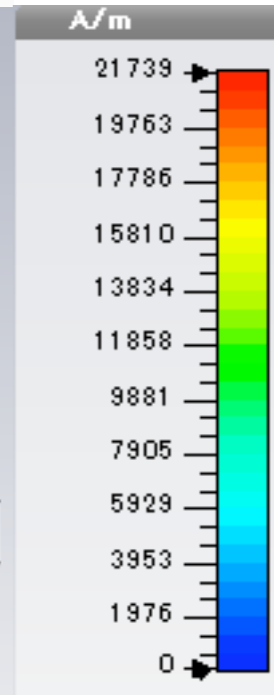
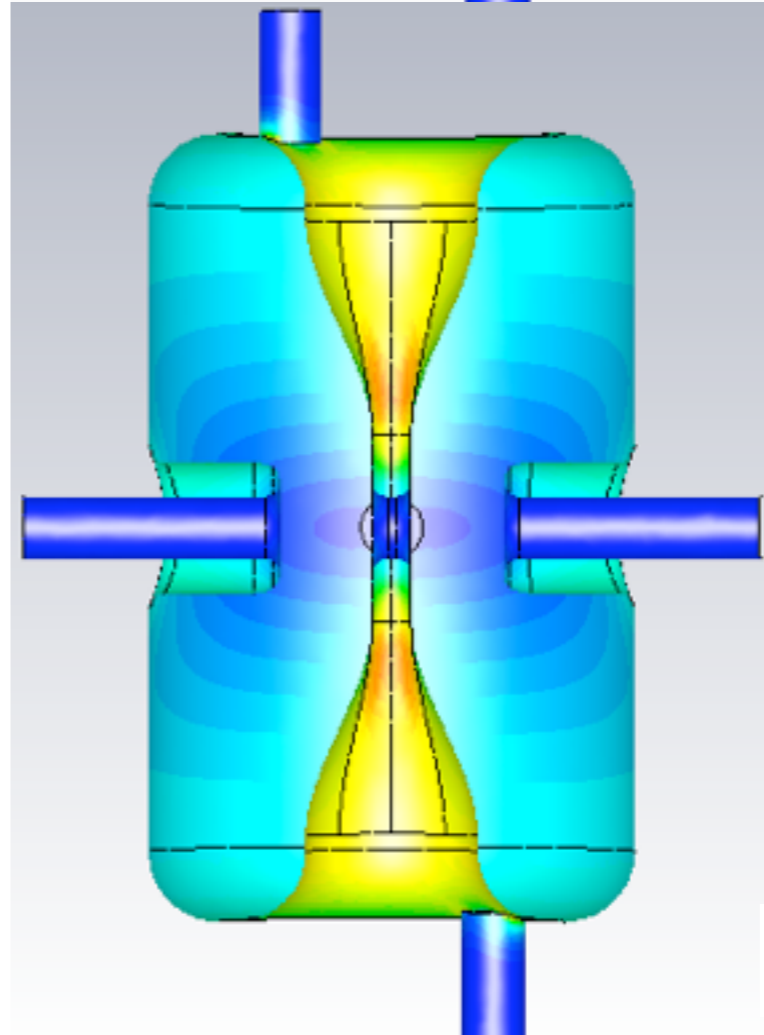
E-field : HWR1



E-field : HWR2

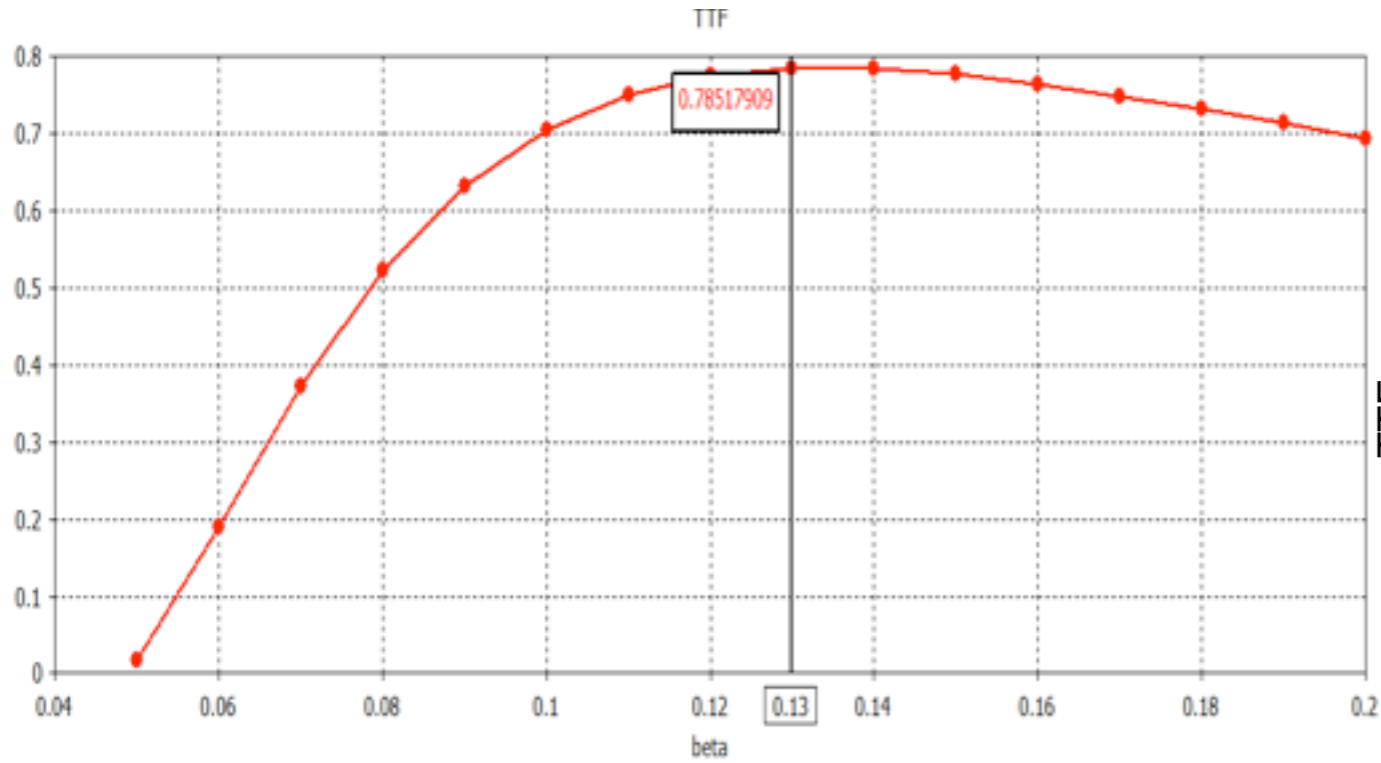


H-field : HWR1

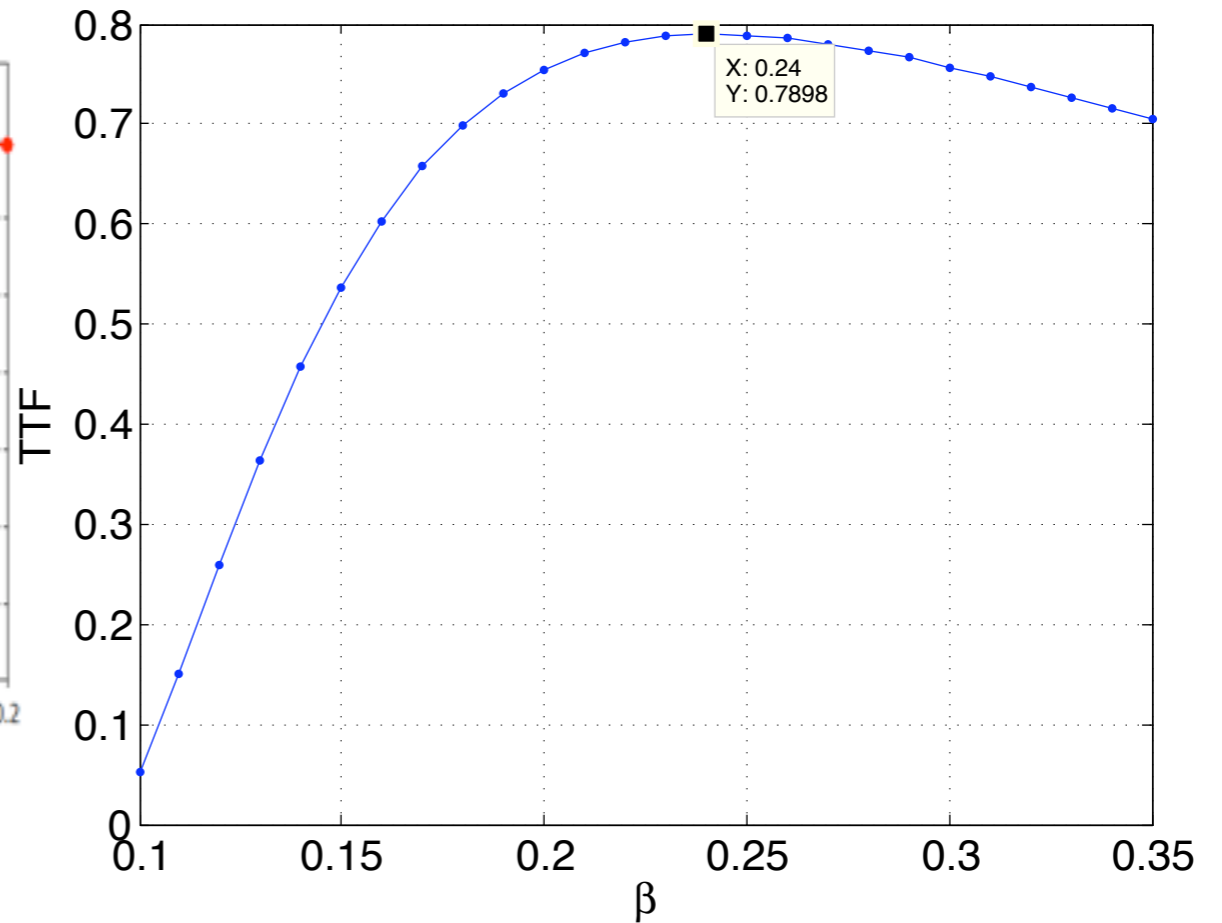


H-field : HWR2

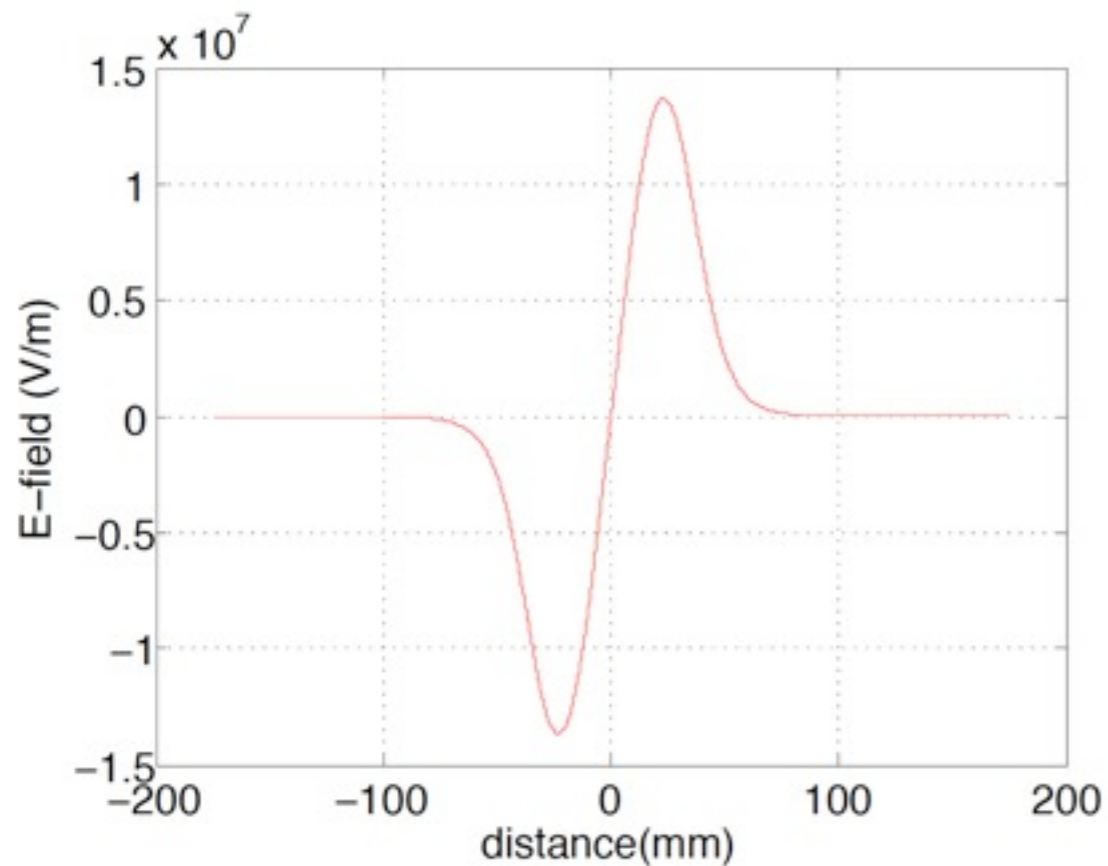
TTF: HWR1



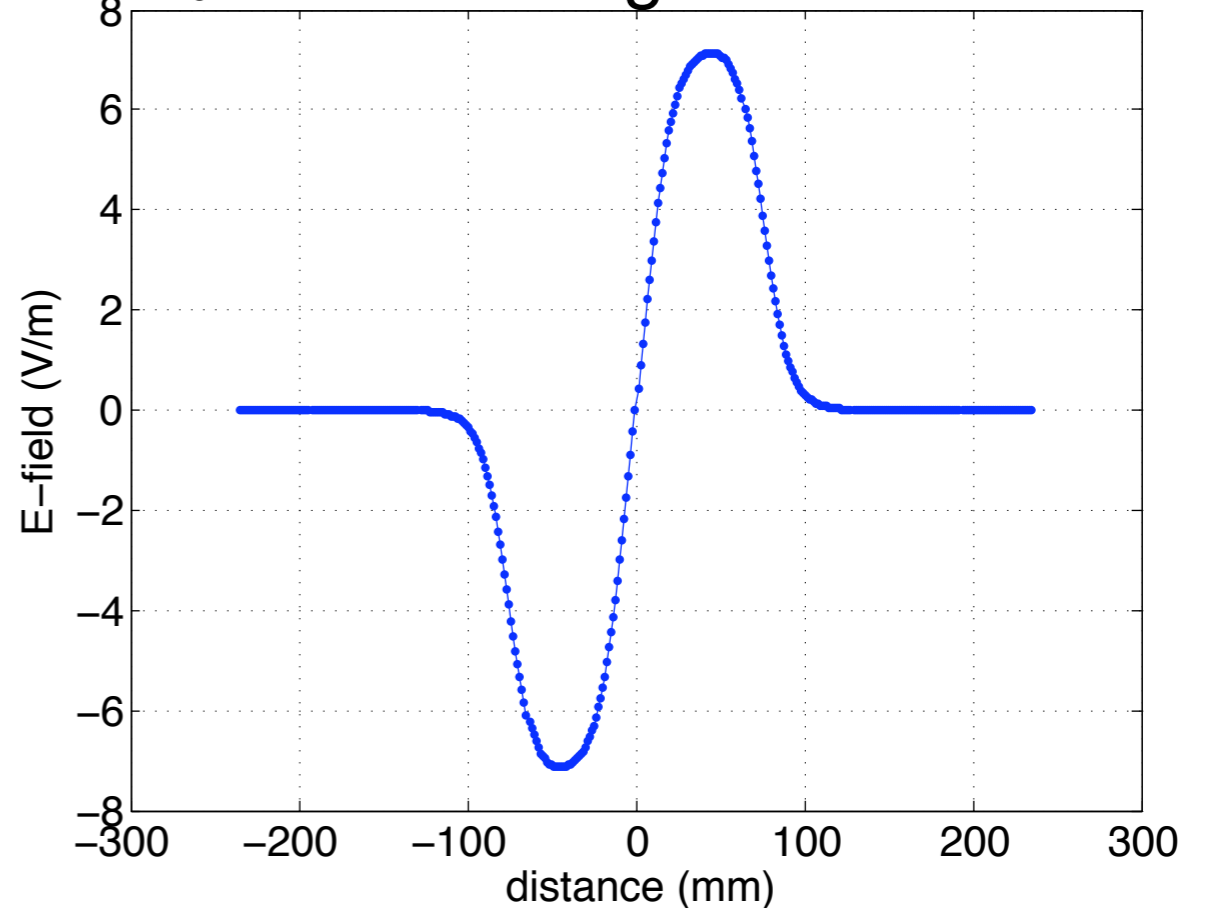
TTF: HWR2



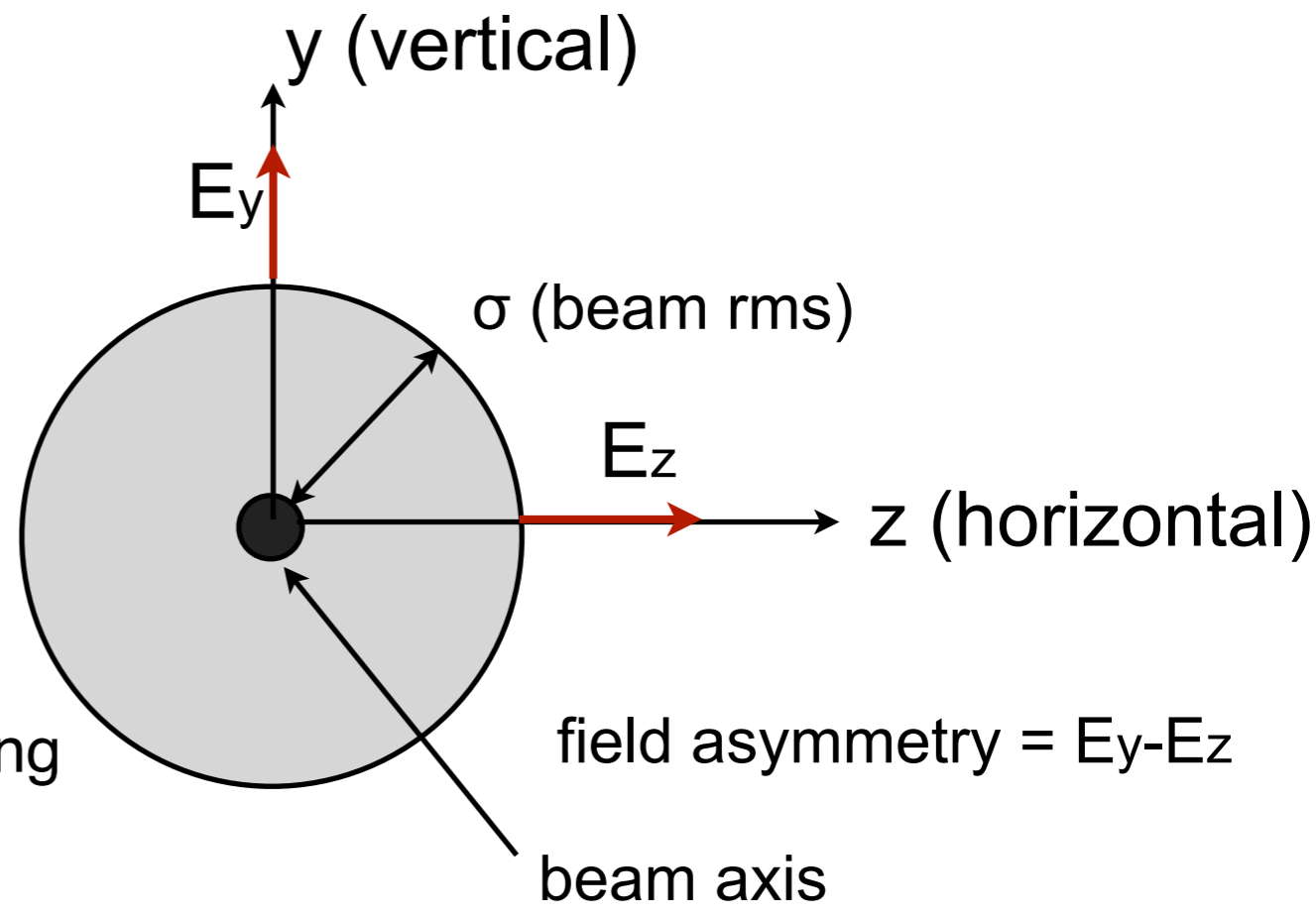
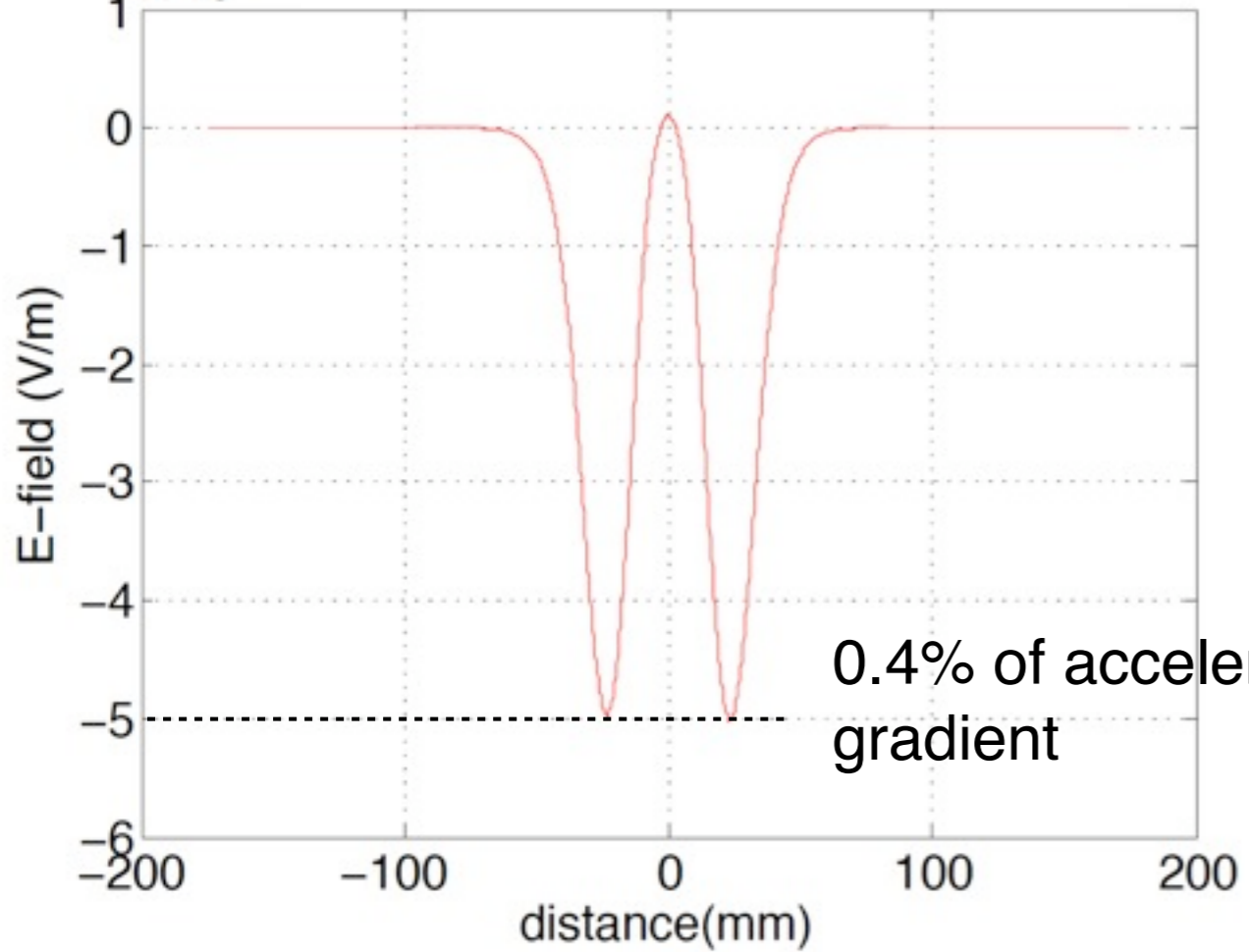
accelerating field: HWR1



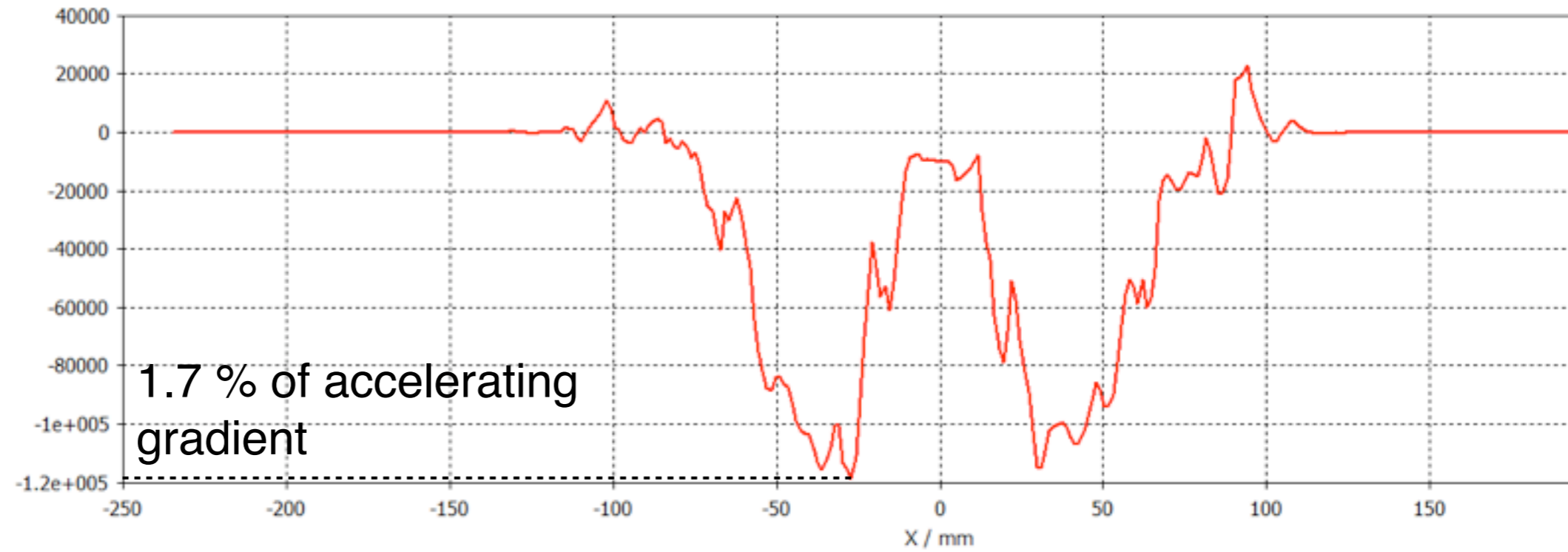
accelerating field : HWR2



field asymmetry : HWR1



field asymmetry : HWR2



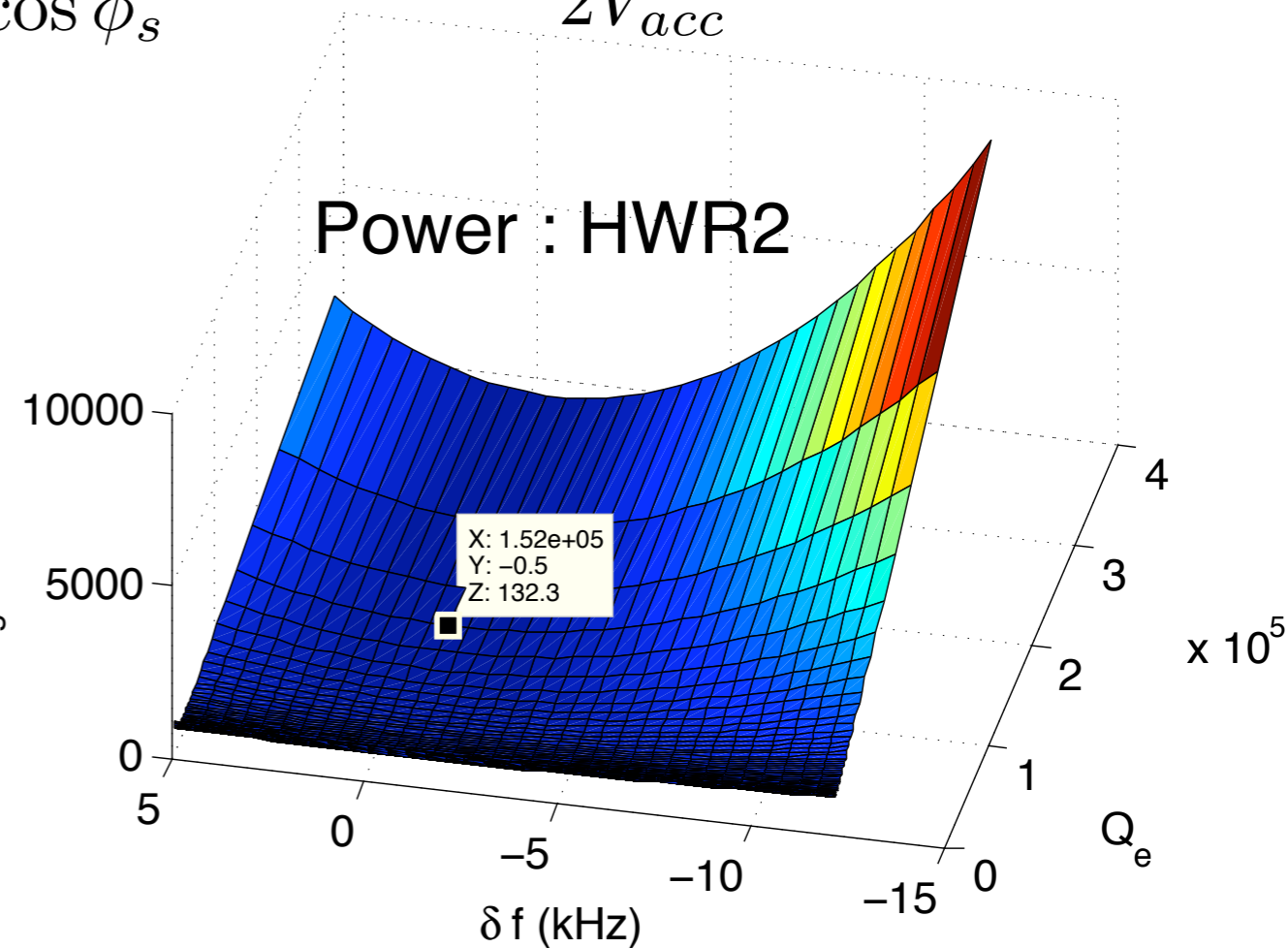
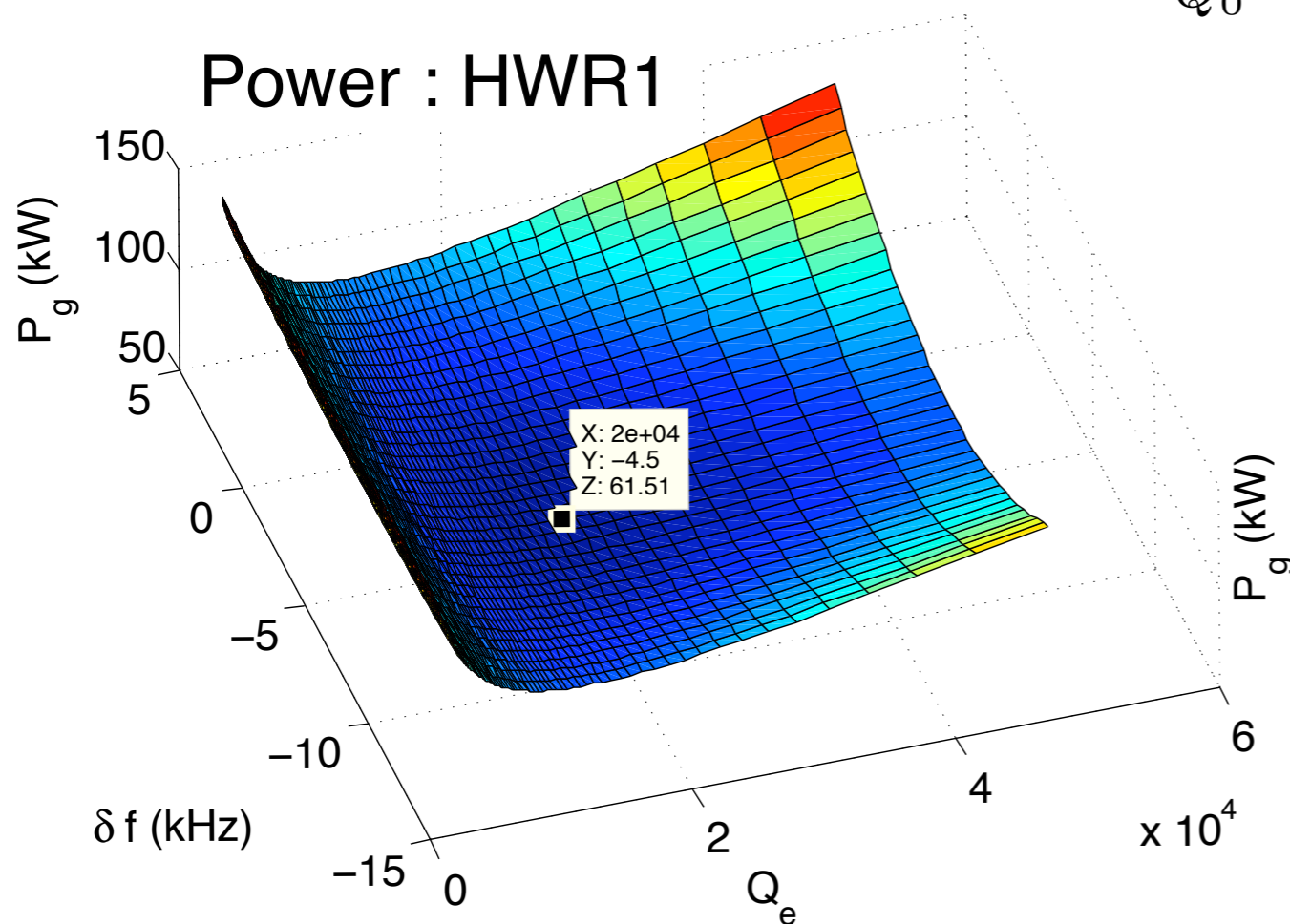
Power supply to the cavity

- The power supply P_g to maintain constant accelerating voltage in strong over-coupling is given as

$$P_g = \frac{V_{acc}^2}{4 \frac{R}{Q_0} Q_L} \left[\left(1 + \frac{R}{Q_0} Q_L \frac{I_b}{V_{acc}} \cos \phi_s \right)^2 + \left(2Q_L \frac{\delta f}{f} - \frac{R}{Q_0} Q_L \frac{I_b}{V_{acc}} \sin \phi_s \right)^2 \right]$$

- The matching condition

$$Q_e \approx \frac{V_{acc}}{I_b \frac{R}{Q_0} \cos \phi_s}, \quad \delta f = \frac{I_b \frac{R}{Q_0} \sin \phi_s}{2V_{acc}} f$$



- The power supply P_g without beam reduces to

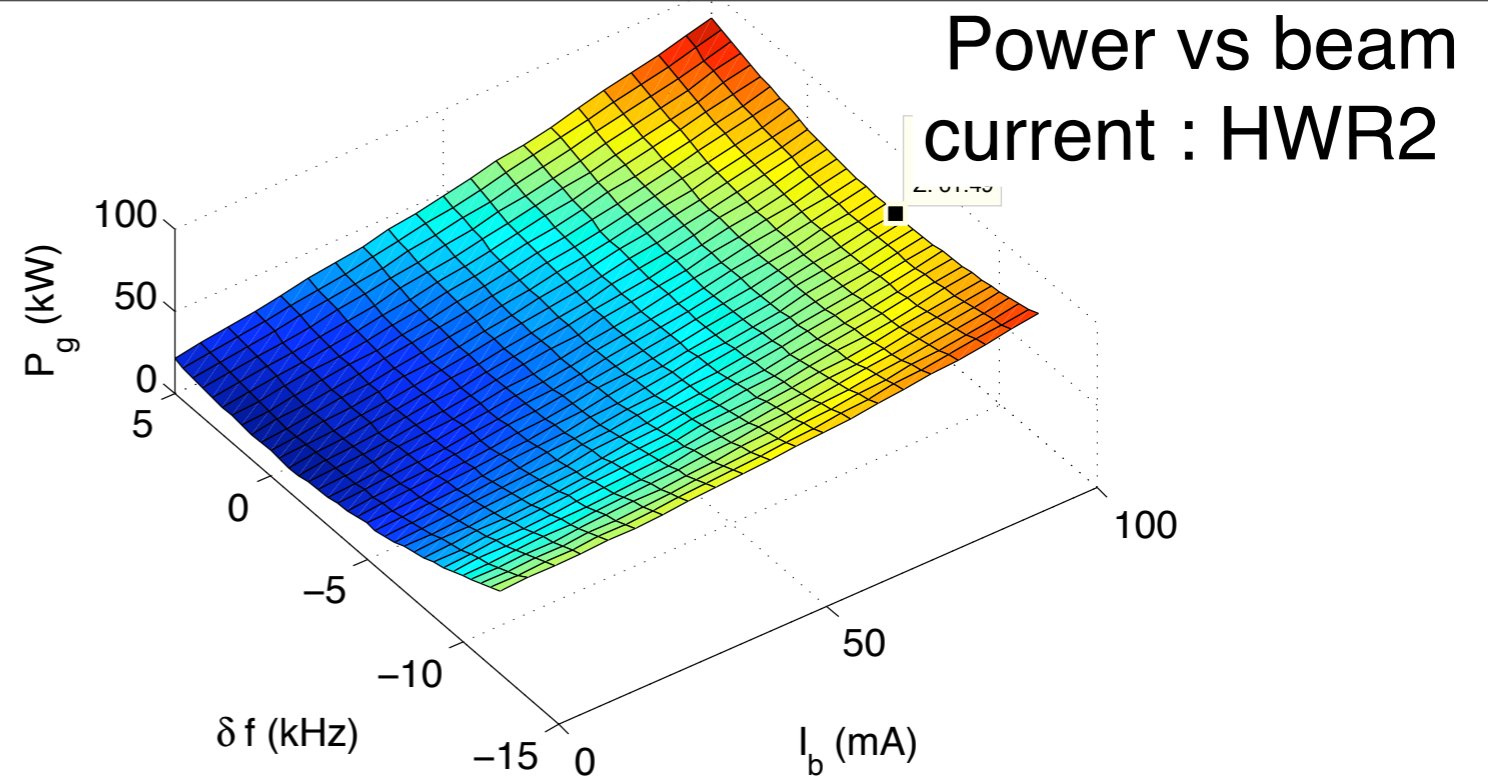
$$P_g = \frac{V_{acc}^2}{4 \frac{R}{Q_0} Q_L} \left[1 + Q_L^2 \left(\frac{2\delta f}{f} \right)^2 \right]$$

On resonance, we have for minimum power

	HWR1	HWR2
adjustable $Q_e=Q_0$	1.6 W	4.8 W
non-adjustable Q_e	44 kW	66 kW

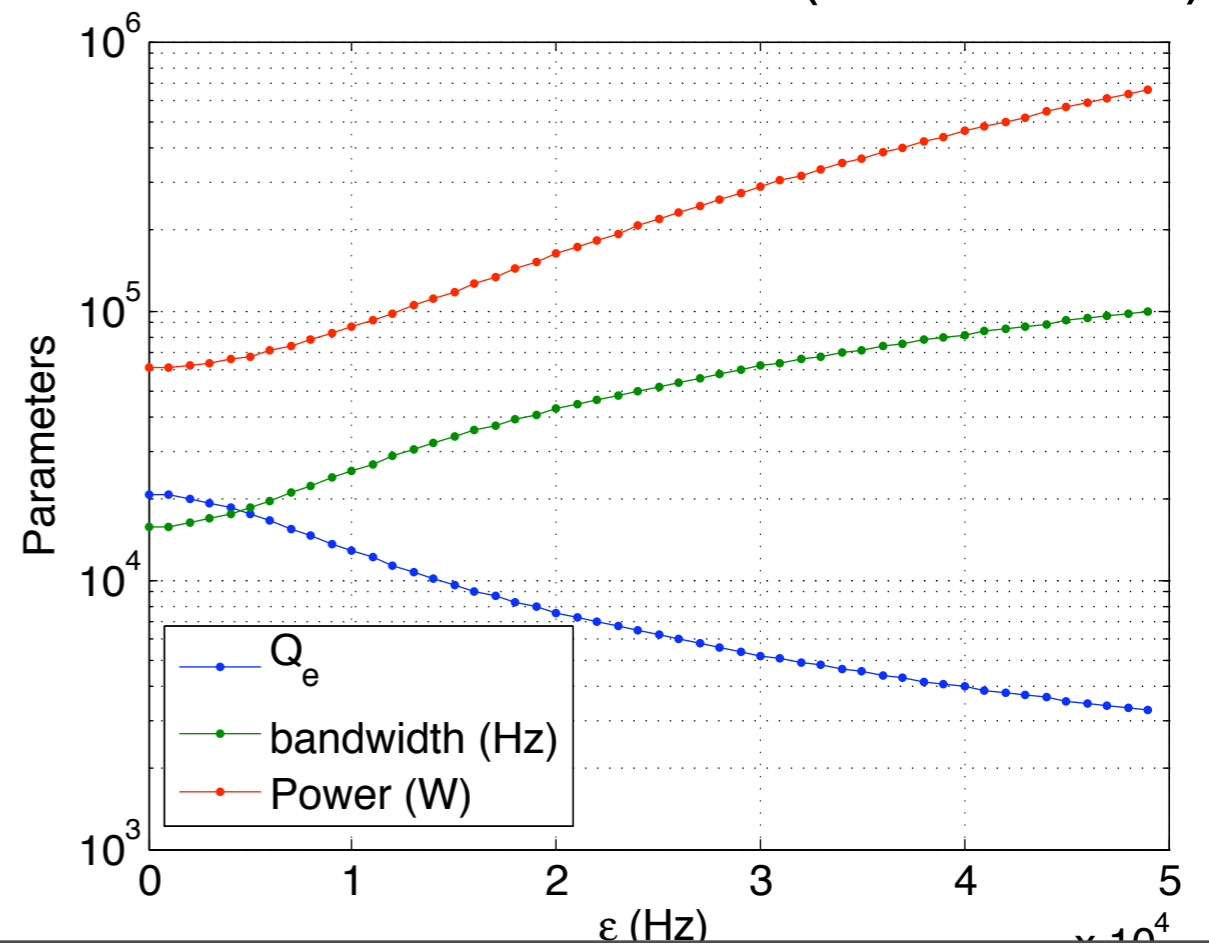
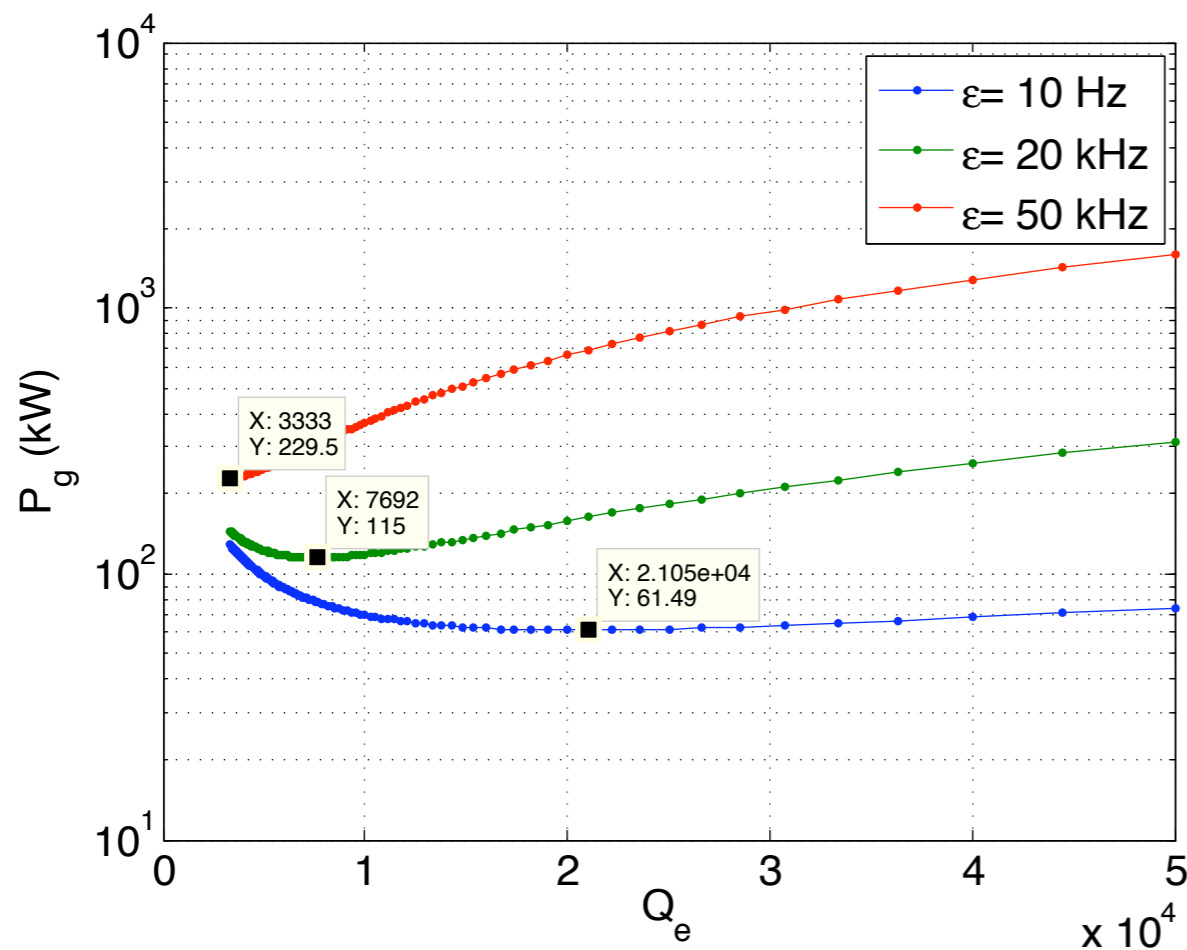
- Beam loading parameters

	HWR1	HWR2
I_b (mA)	100	100
ϕ_s (°)	-30	-30
Q_e	2.10E+04	1.45E+05
f_{detune} (kHz)	-4.5	-0.65
$\Delta_{\pm 3dB}$ (kHz)	15.7	2.37
P_g (kW)	62	132



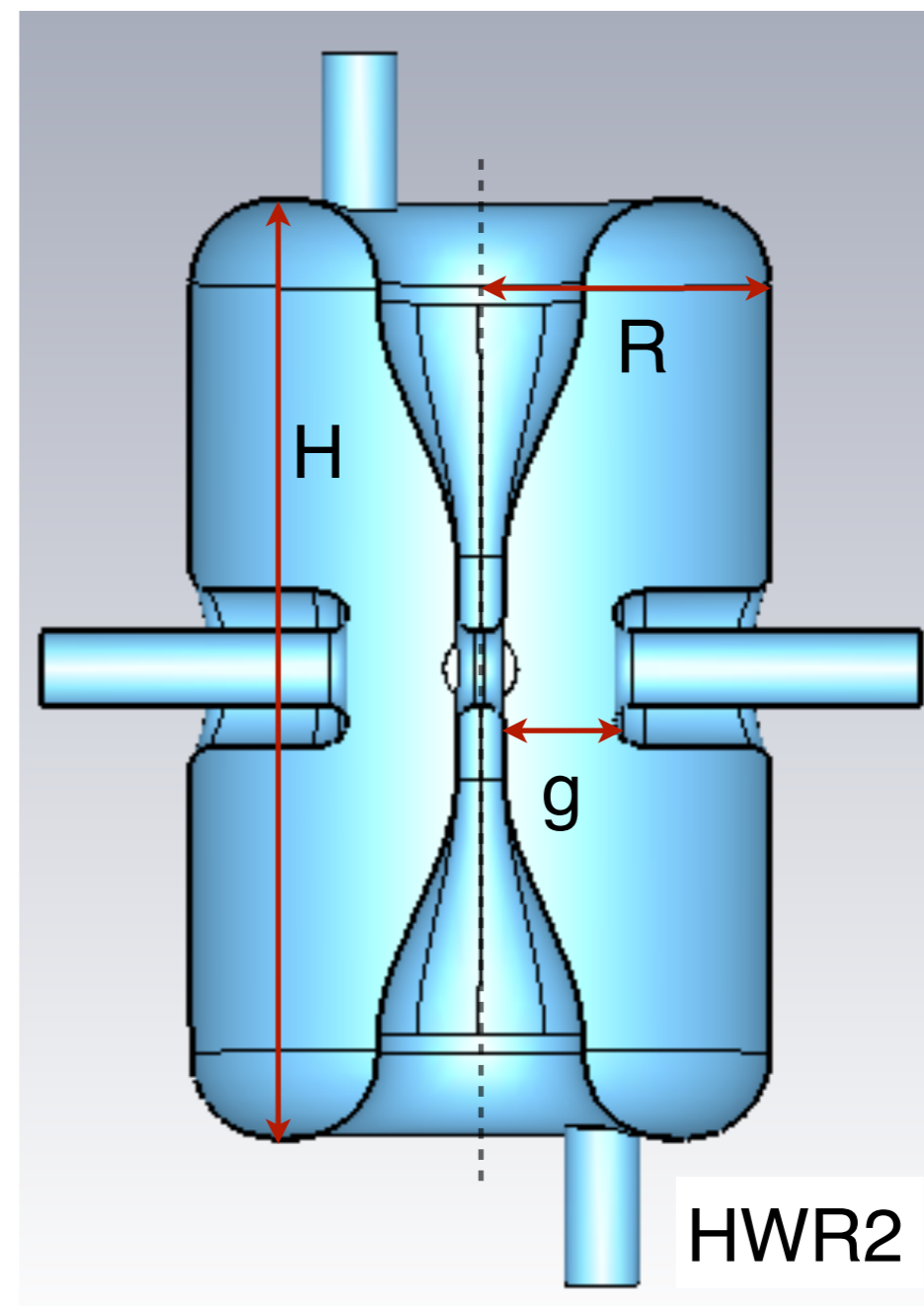
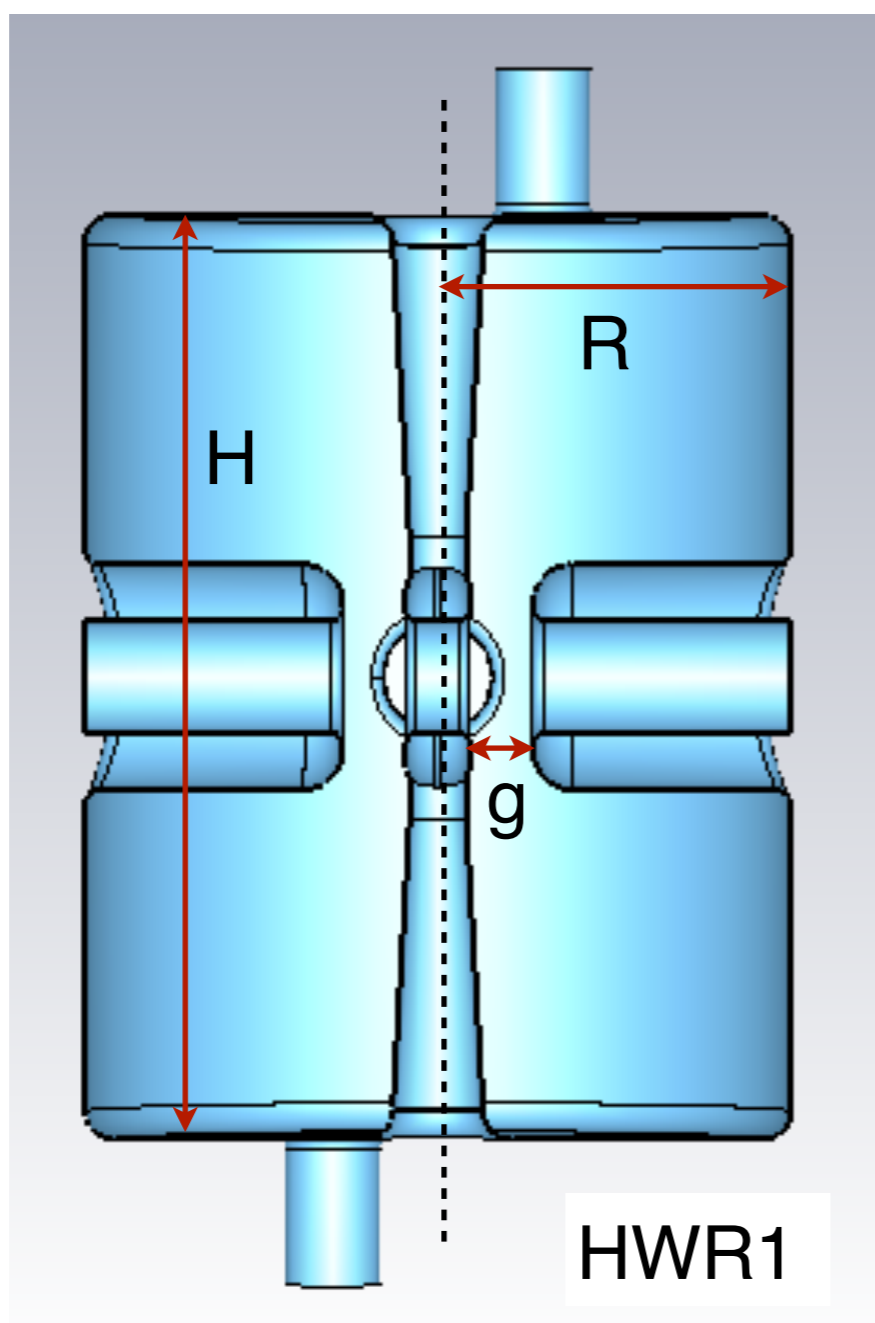
- Power with frequency shift ε (after detuning)

$\varepsilon_{\text{LFD}} = 65 \sim 380$ Hz (stiffened)
35 kHz (unstiffened)

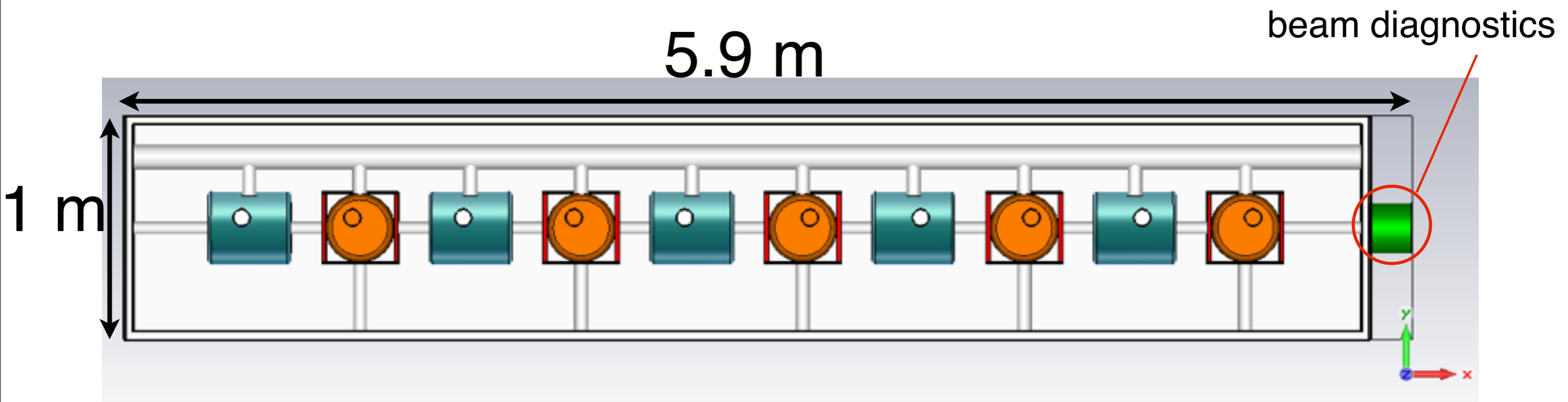
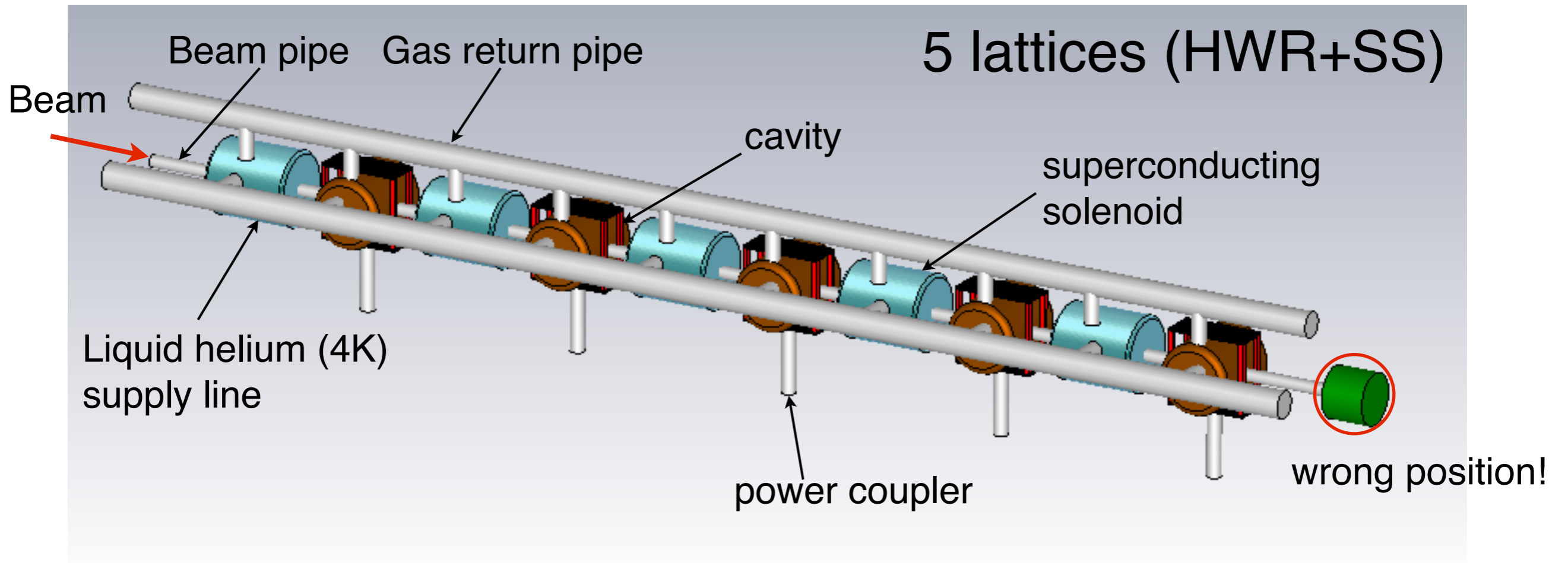


Fabrication error

freq. shift	HWR1	HWR2
df/dH (MHz/mm)	-0.8684	-0.5972
df/dg (MHz/mm)	4.4115	1.1815
df/dR (MHz/mm)	-0.7316	-0.7992



Cryomodule configuration



Conclusion

- Fron end design is now done with target specification of each component.
- Electromagnetic design of the two superconducting half wave resonators is complete. Their prototypes will be fabricated soon.
- Design values are close to the target values (Accelerating voltage).
- The multipaction study of the cavities are still under way.